

RAFT

Radar Fence Transponder

Preliminary Design Review

19 Nov04

MIDN 1/C Eric Kinzbrunner

MIDN 1/C Ben Orloff

MIDN 1/C JoEllen Rose



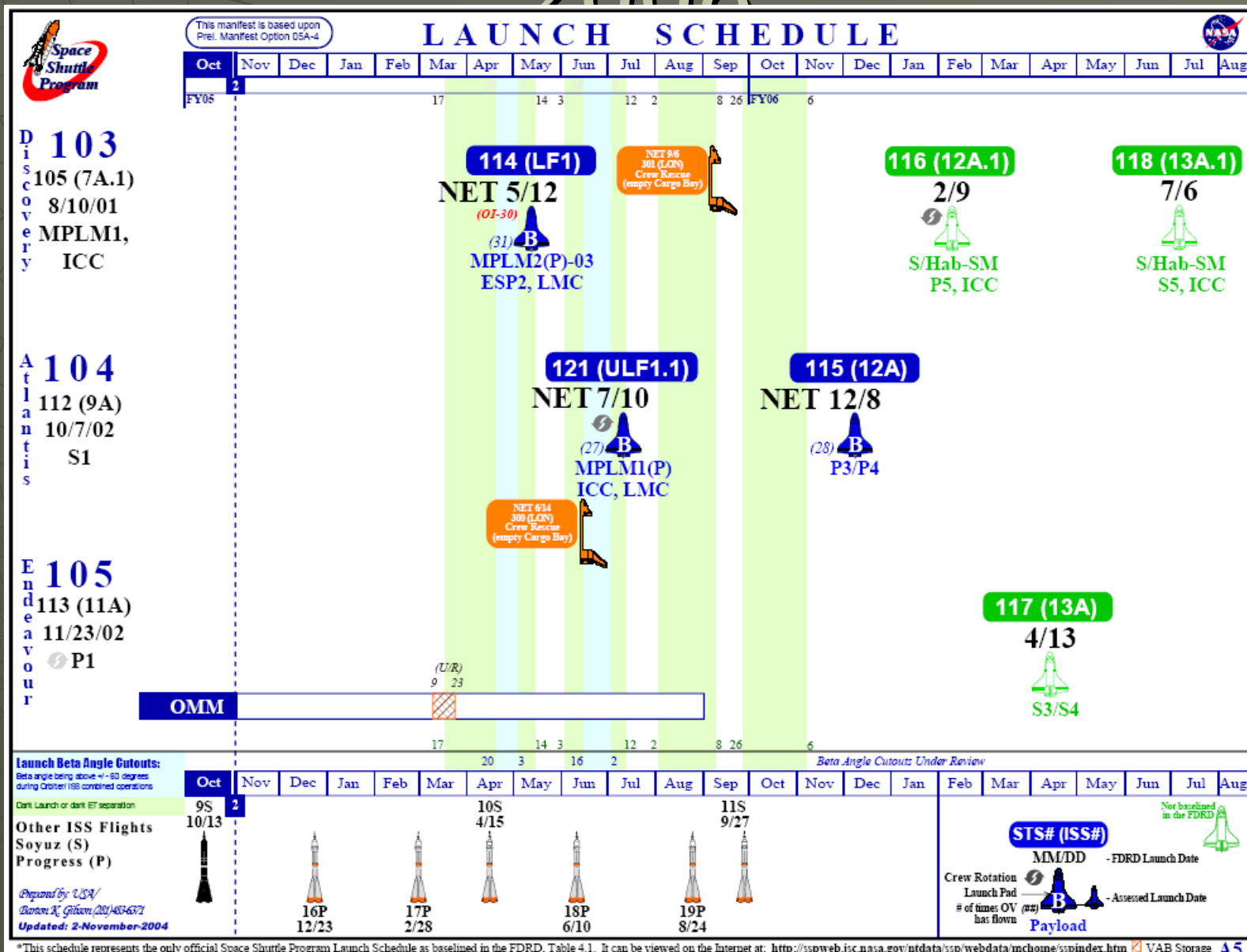
OLAW RAFT Team

- ◆ Chief Of Integration & Ops: Capt Yvonne Fedee
- ◆ Payload Manager: Mr Perry Ballard
- ◆ Back Up Payload Manager: Lt Reann Caldwell
- ◆ Payload Integration Engineer(PIE): Mr Carson Taylor
- ◆ Launcher & Back Up PIE: Mr Scott Ritterhouse
- ◆ Safety Engineer (SE): Ms. Theresa Shaffer
- ◆ Launcher & Back up SE: Mr Darren Bromwell

Key Milestones: Tentative Schedule

- ◆ Assumption: Launch NET December 2005
- ◆ RAFT Kickoff Apr 04
- ◆ RAFT USNA SRR Sep 04
- ◆ **RAFT PDR** **19 Nov 04**
- ◆ Launcher CDR Nov 04
- ◆ RAFT Phase 0/1 Safety Dec 04
- ◆ RAFT CDR Feb 05
- ◆ RAFT Phase 2 Safety Feb 05
- ◆ RAFT Flight Unit Delivery May 05
- ◆ RAFT Phase 3 Safety Aug 05
- ◆ RAFT Delivery/Install Oct 05
- ◆ RAFT Flight (STS-116) NET Feb 06

Shuttle Manifest: 2004 - 2008

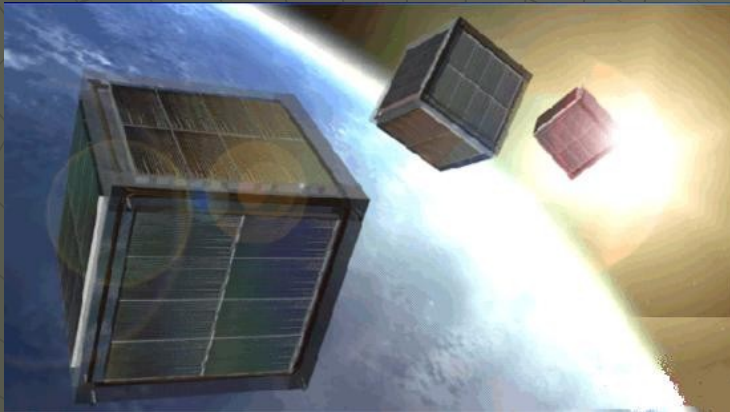


*This schedule represents the only official Space Shuttle Program Launch Schedule as baselined in the FDRD, Table 4.1. It can be viewed on the Internet at: <http://sspweb.jsc.nasa.gov/ntdata/ssp/webdata/mchome/sspindex.htm> VAB Storage A5

Background

30 to 50 in Construction

How to Track them???



**AIAA/US
USmall
Sat
Conferen
ce**

**30% of
papers
were for
PICO,
NANO
and
CUBEsat
s**

All

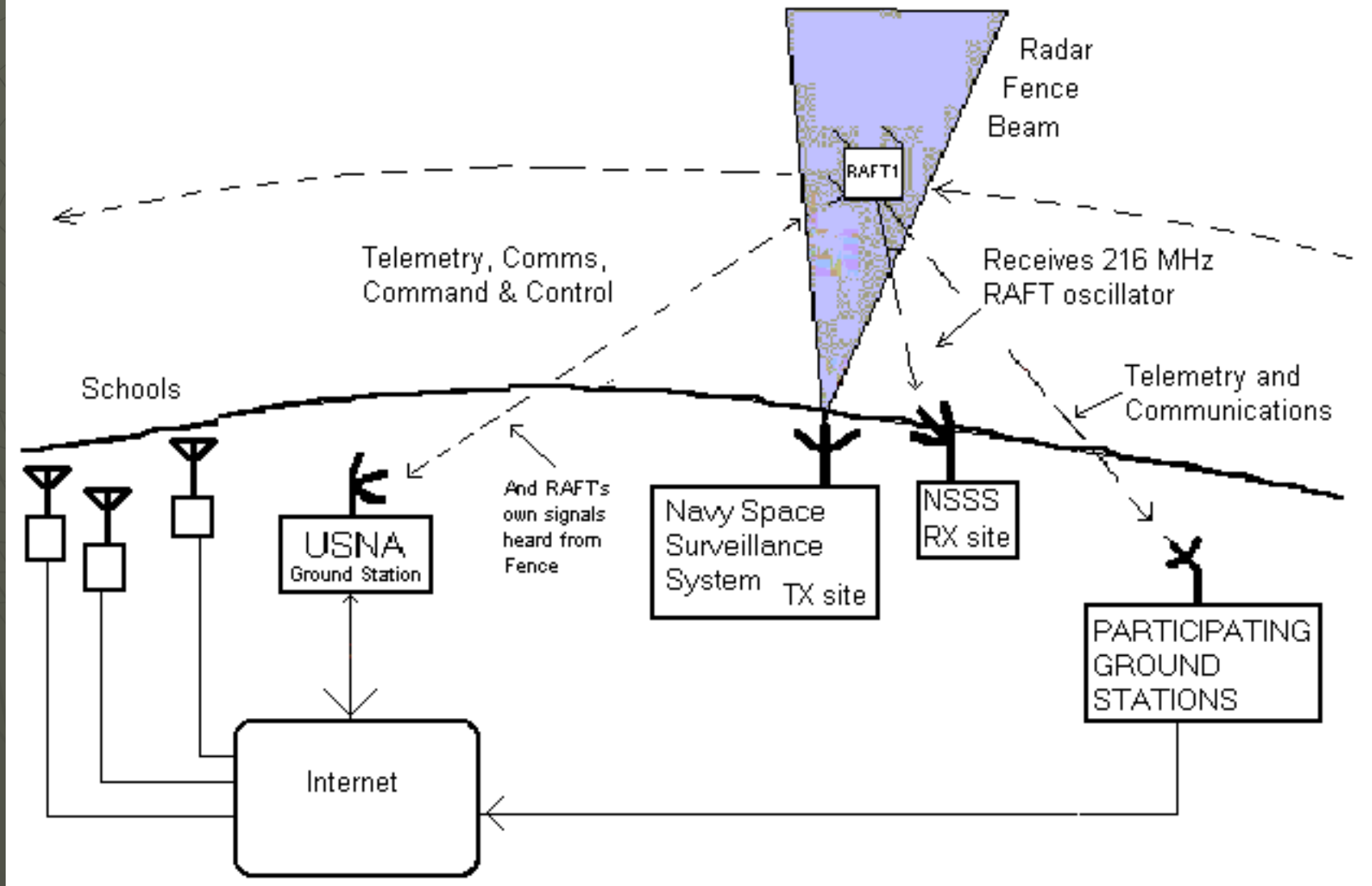


Mission Statement

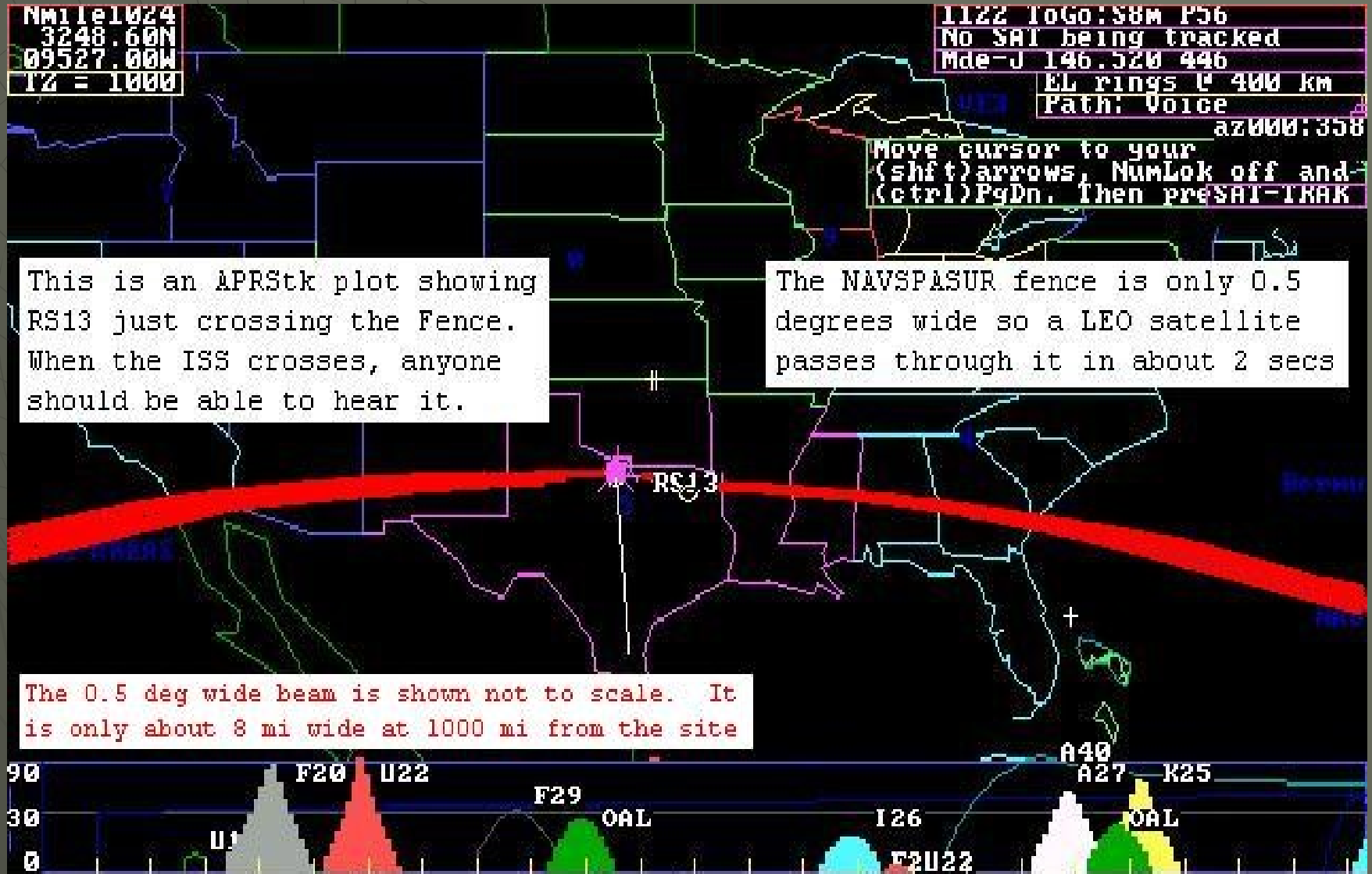
The mission of RAFT is:

- ◆ To provide the Navy Space Surveillance (NSSS) radar fence with a **means to determine the bounds** of a constellation of PicoSats otherwise undetectable by the radar fence
- ◆ To enable NSSS to independently **calibrate their transmit and receive beams** using signals from RAFT.
- ◆ This must be accomplished with **two PicoSats**, one that will actively transmit and receive, and one with a passively augmented radar cross-section.
- ◆ Additionally, RAFT will provide experimental **communications transponders** for the Navy Military Affiliate Radio System, the United States Naval Academy's Yard Patrol crafts, and the Amateur Satellite Service.

RAFT1 Mission Architecture



NSSS Radar Fence



NSSS Radar Fence

Transmit Power: 768 kW of power from Lake Kickapoo, TX

Antenna Gain: About 30dB

Transmission Sites: Lake Kickapoo, Texas

Jordan Lake, Alabama

Gila River, Arizona

Receiving Sites: San Diego, California

Elephant Butte, New Mexico

Red River, Arkansas

Silver Lake, Mississippi

Hawkinsville, Georgia

Tattnall, Georgia

RAFT1 and MARScom

RAFT1 Satellite

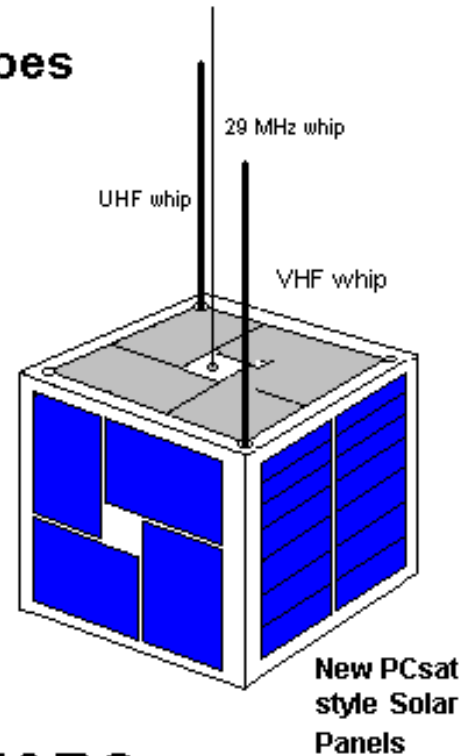
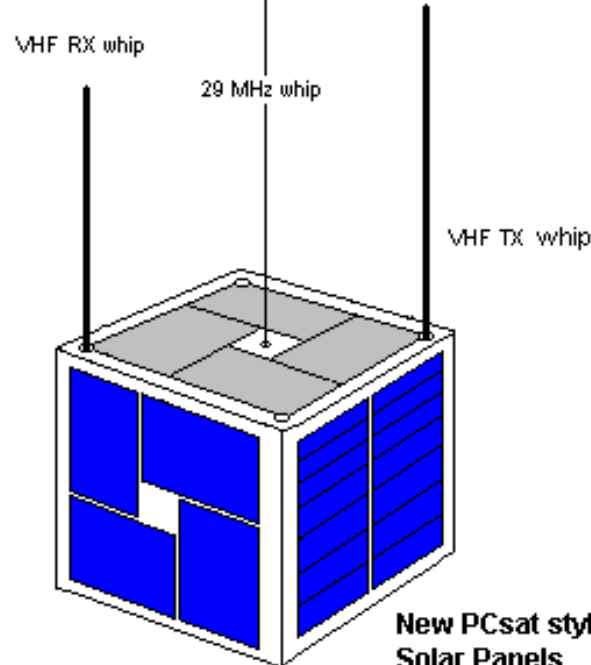
5" cubes

Downlink:

145.825 MHz Audio with both
AX.25 Packet and PSK-31 signals

Uplinks:

29.4 MHz linear PSK-31
145.825 AX.25 Packet



MARScom

Power Budget:

1 Watt orbit average DC power

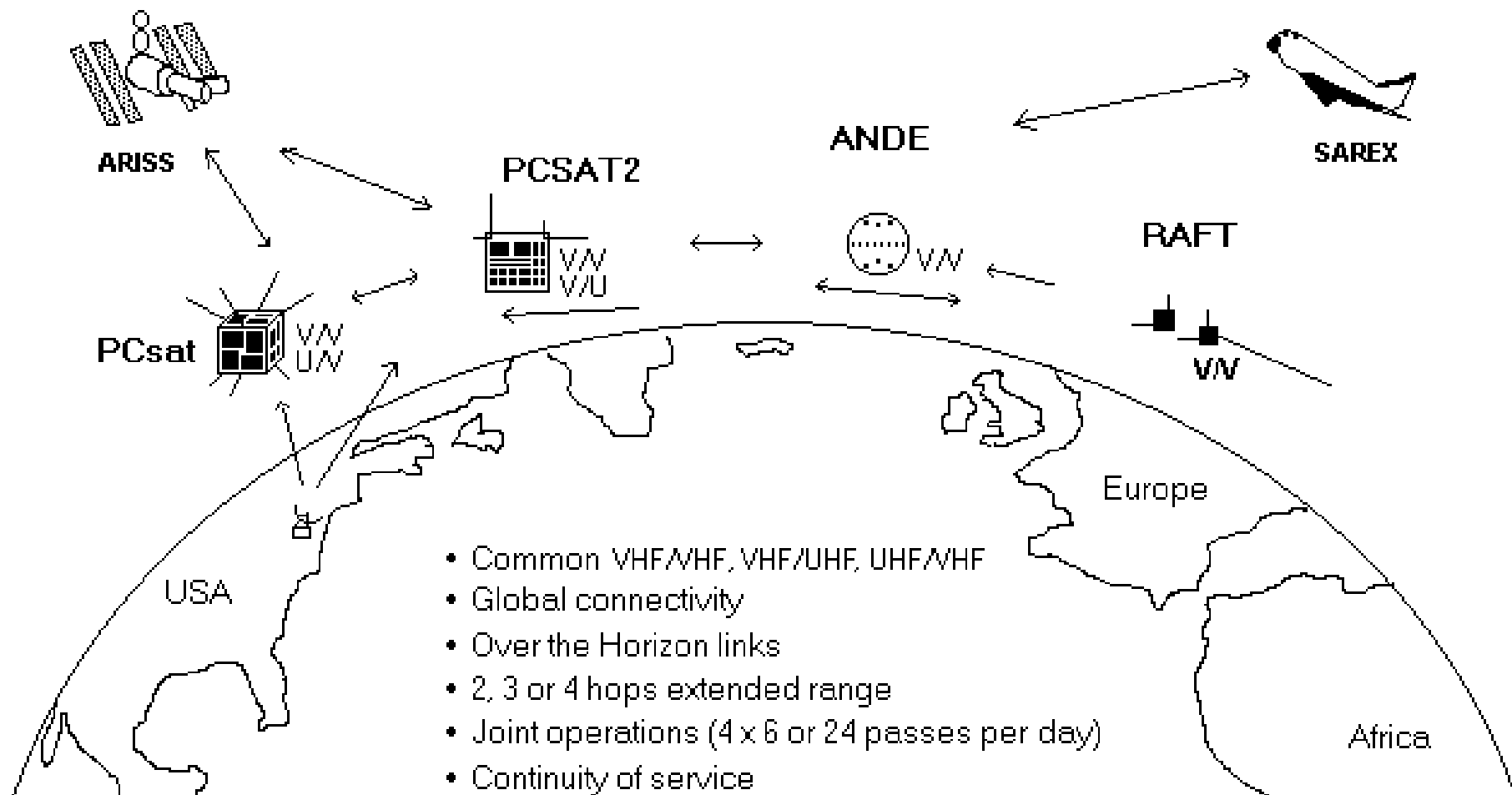
Link Budget:

10W UHF AM xmtr Voice uplinks
Downlink to any HF receiver
Omni Antennas for ground user

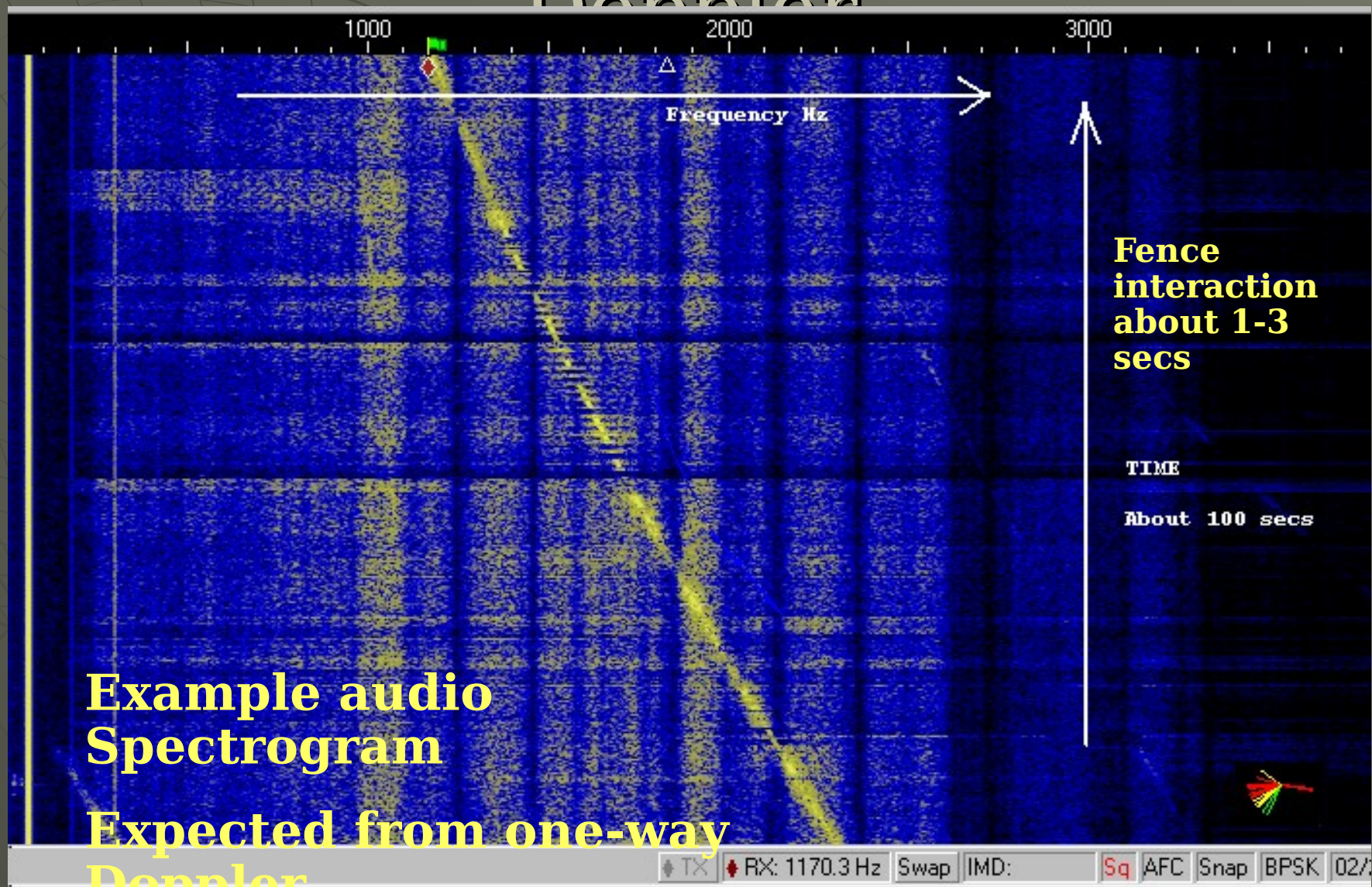
Channels:

UHF AM uplink
VHF FM uplink
HF SSB downlink

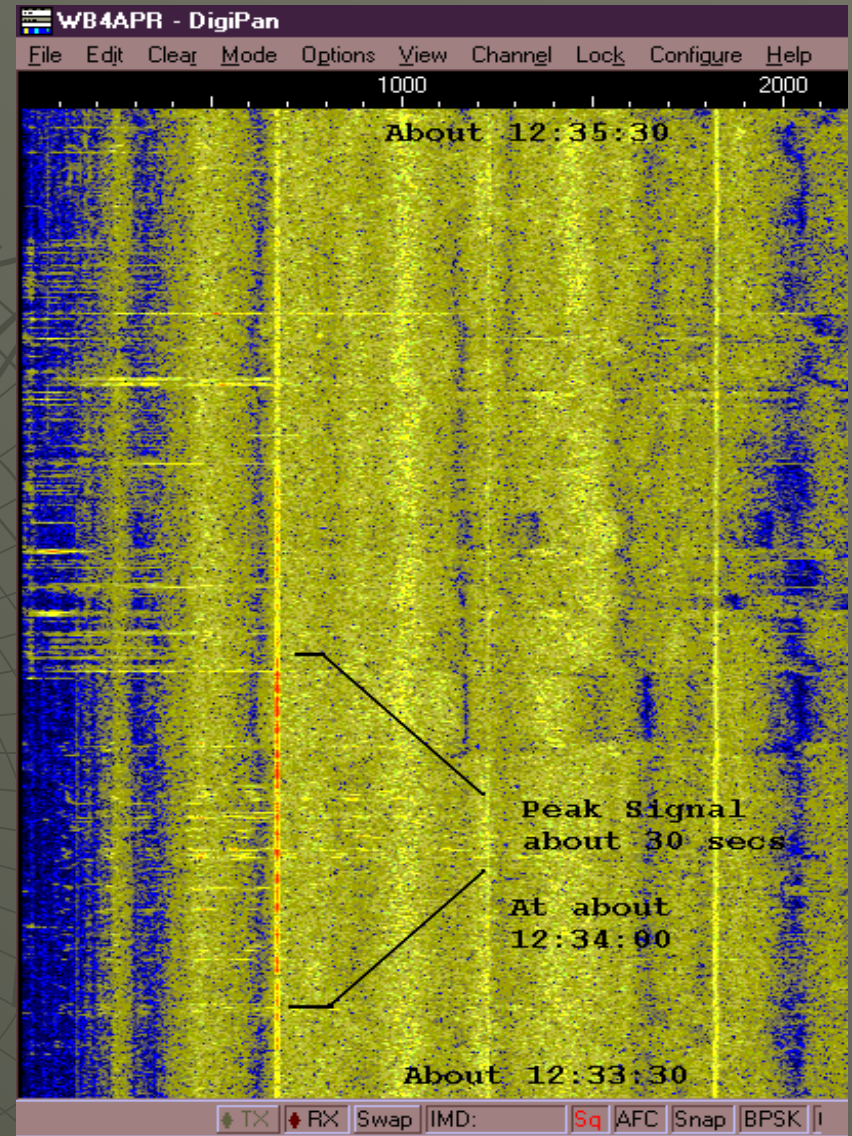
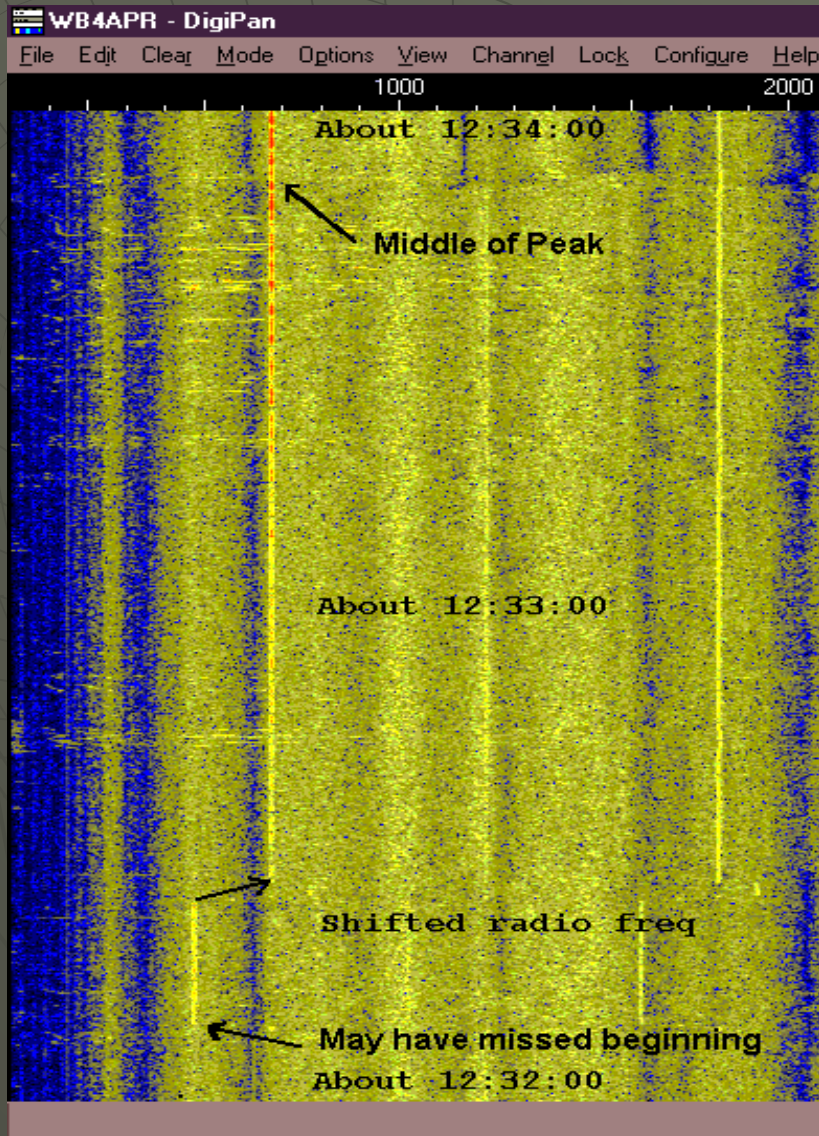
Constellation Operation of USNA Satellites



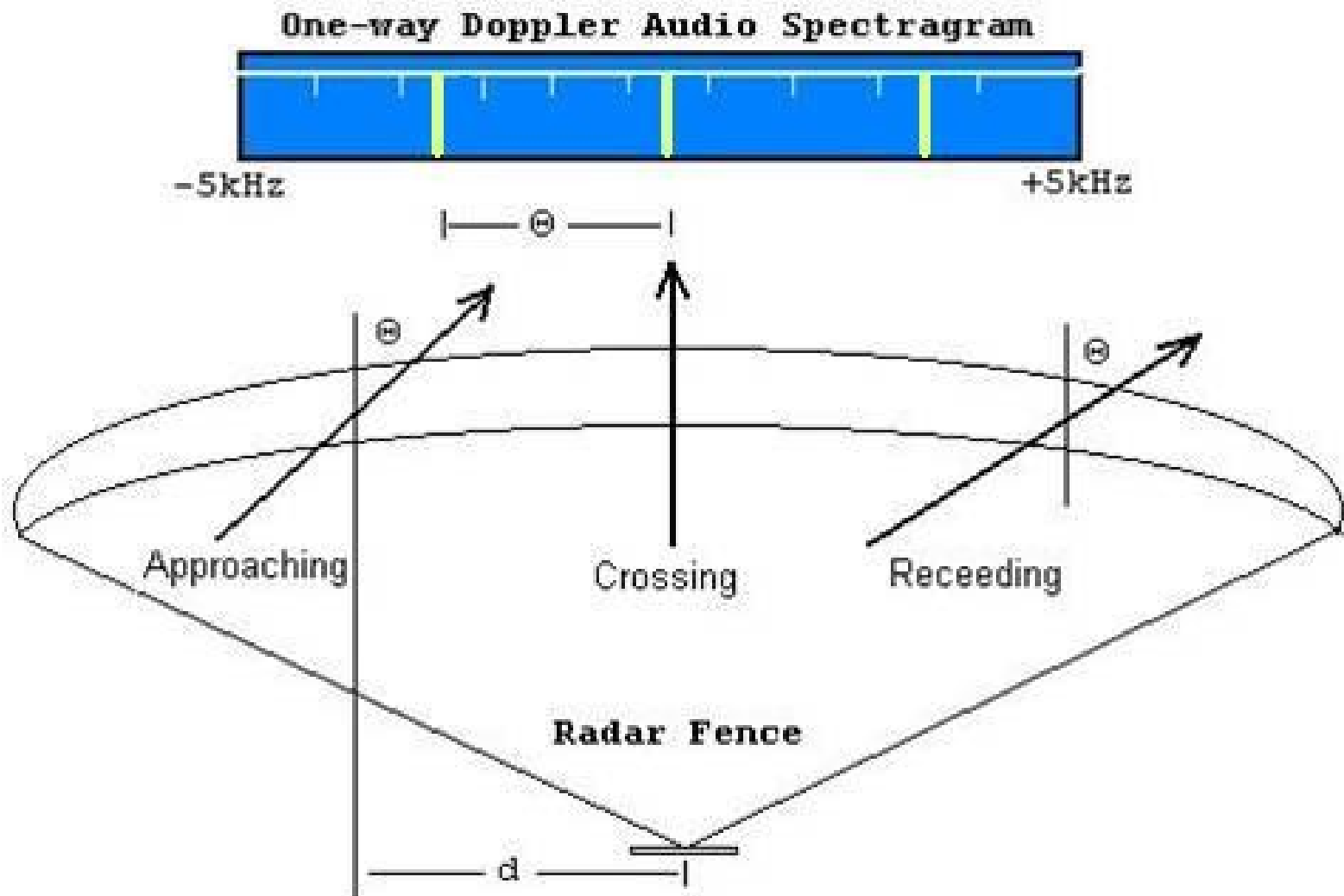
Spectrogram of Satellite Doppler



NSSS / Moon Intercept

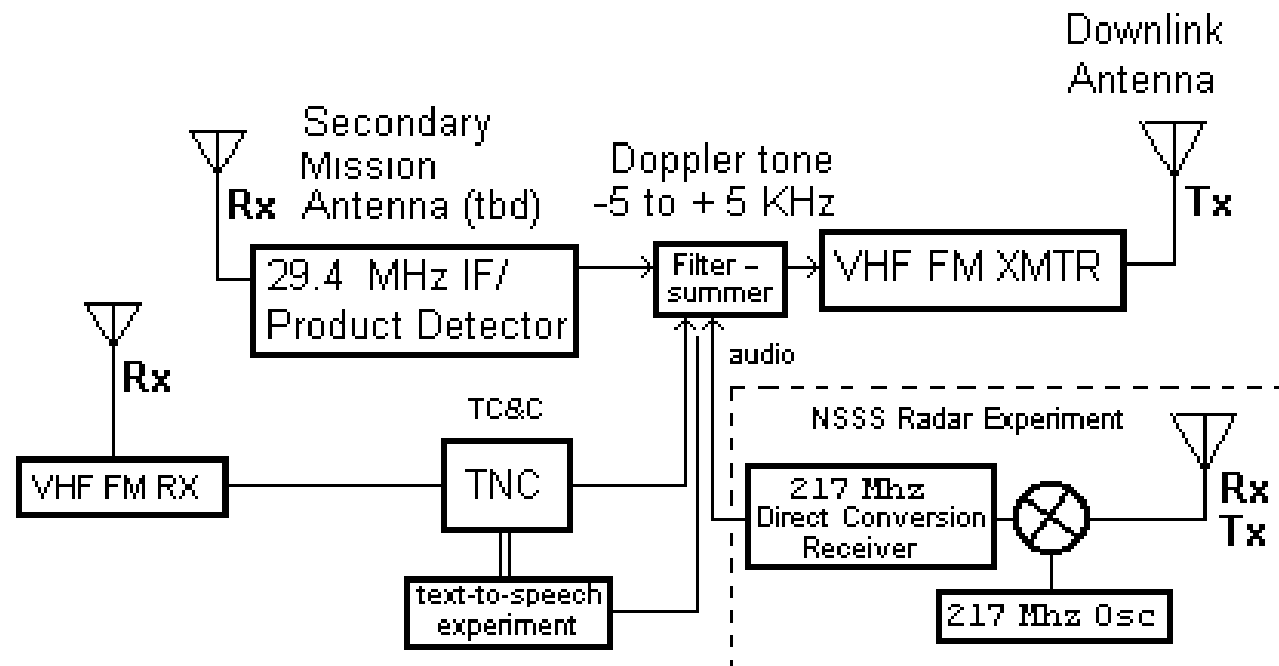


Pass Geometry



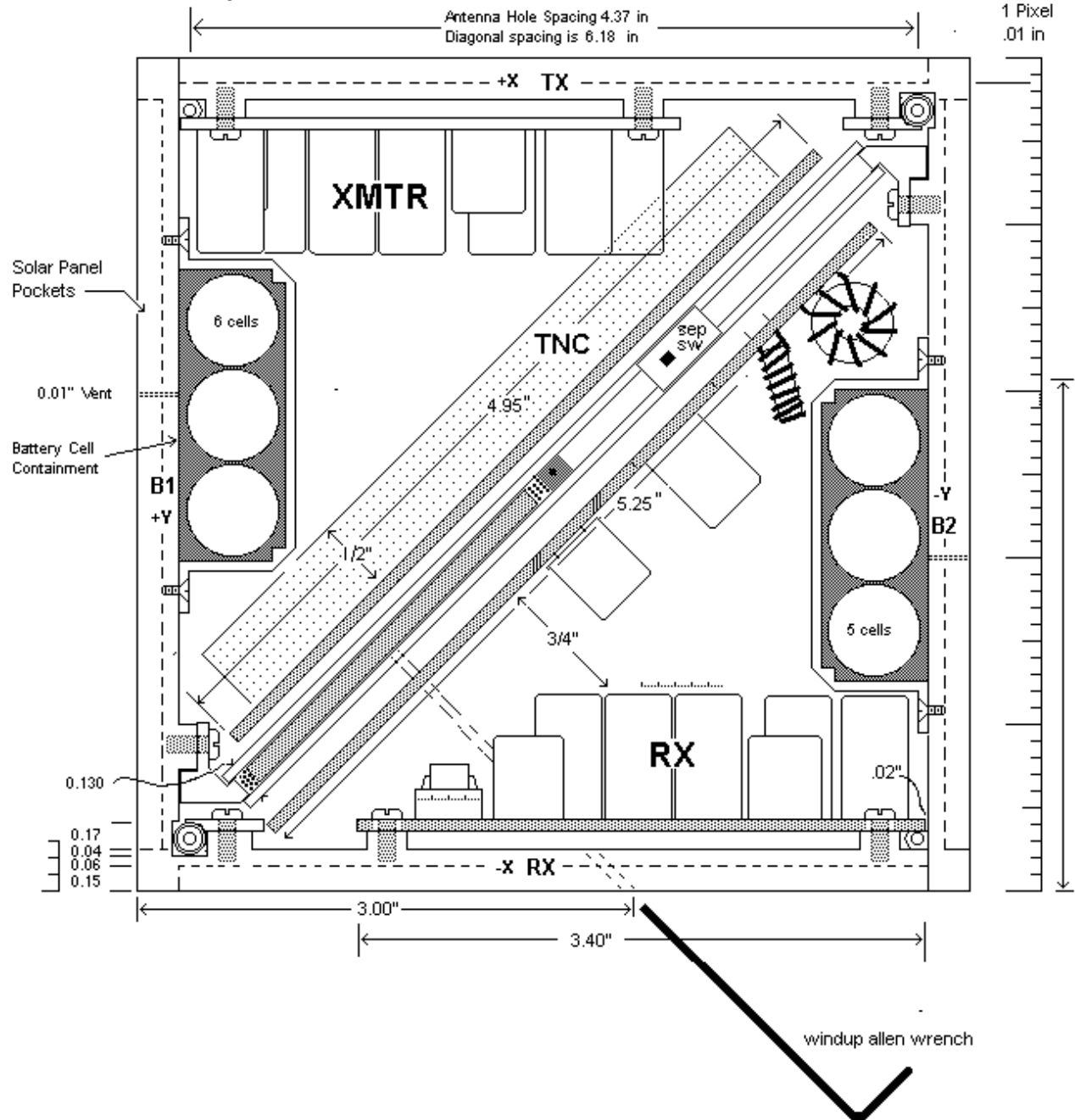
Raft1 Block Diagram

RAFT1 Radar Fence Transponder

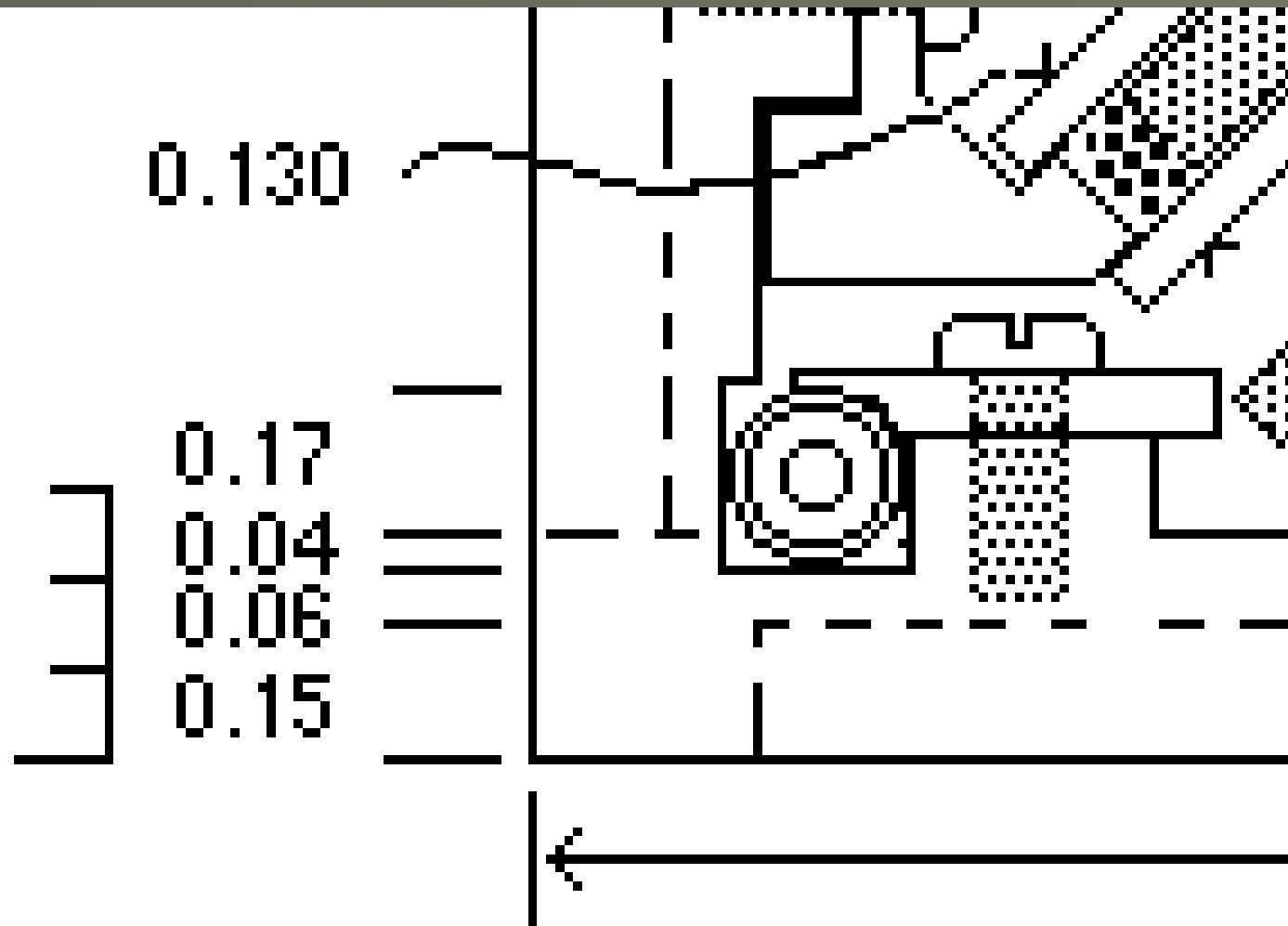


RAFT1 Internal Diagram Top View

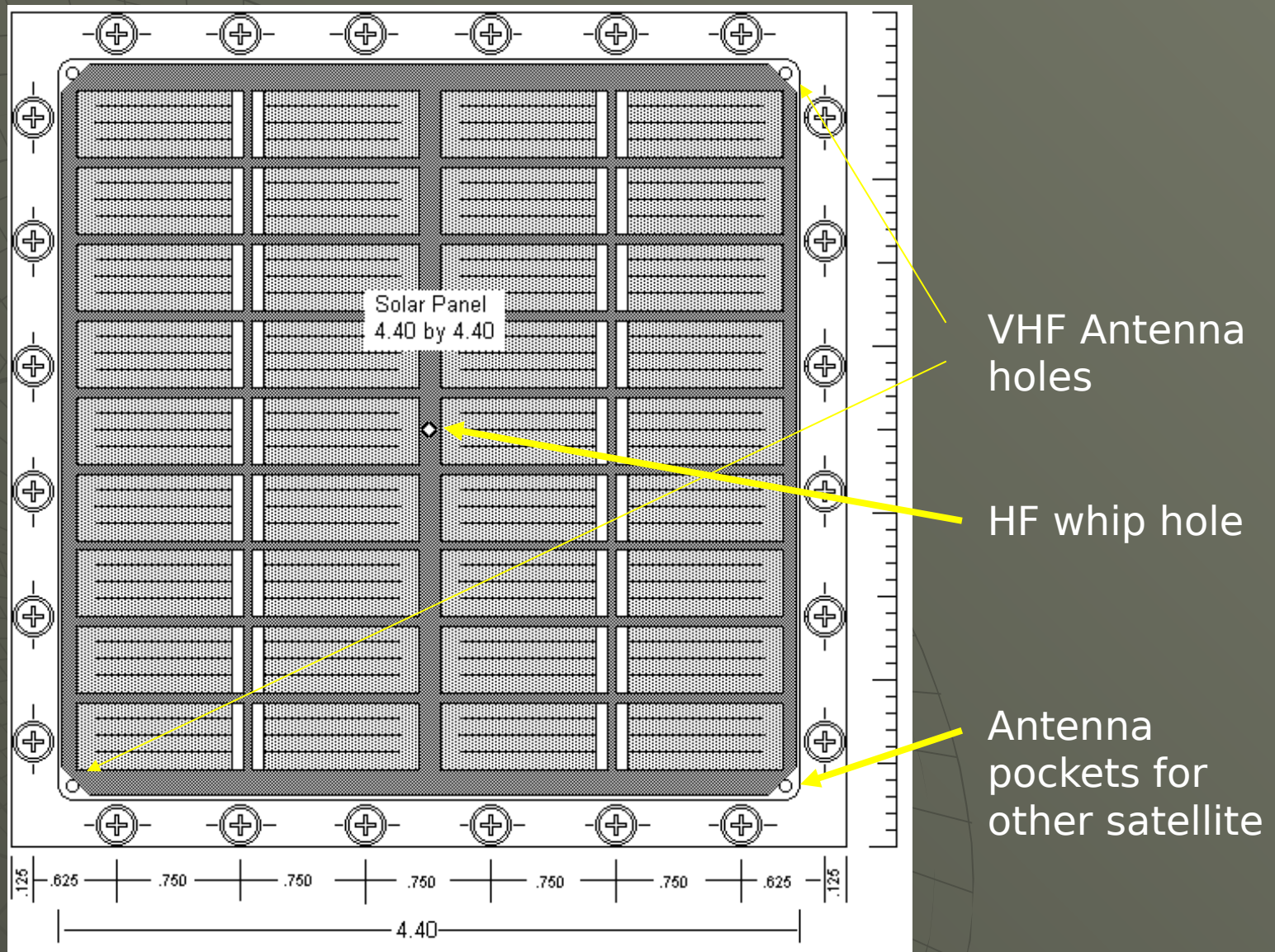
+Z is the ANT panel
-Z is the CONNECTOR panel



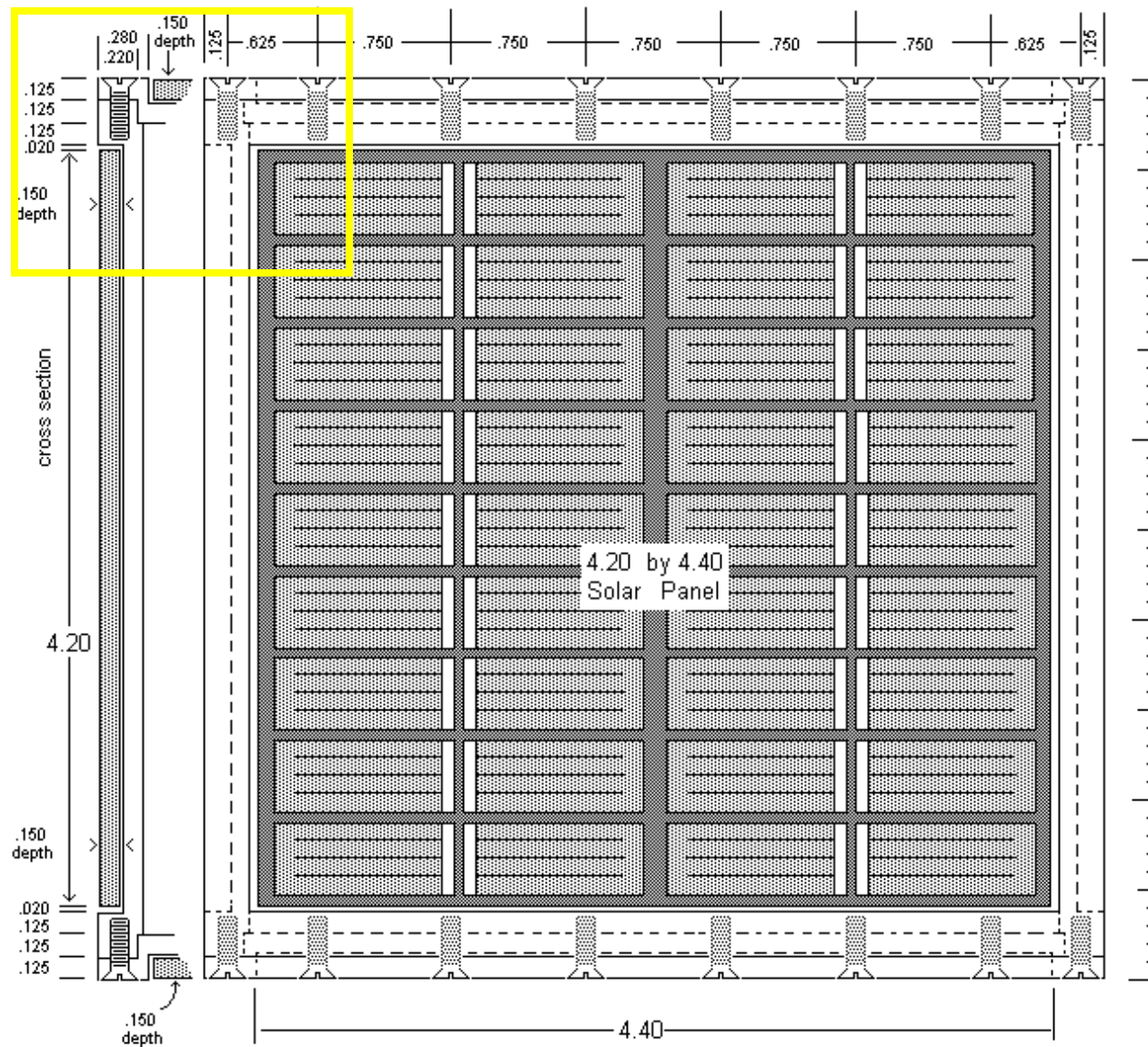
RAFT Internal Diagram Corner Detail



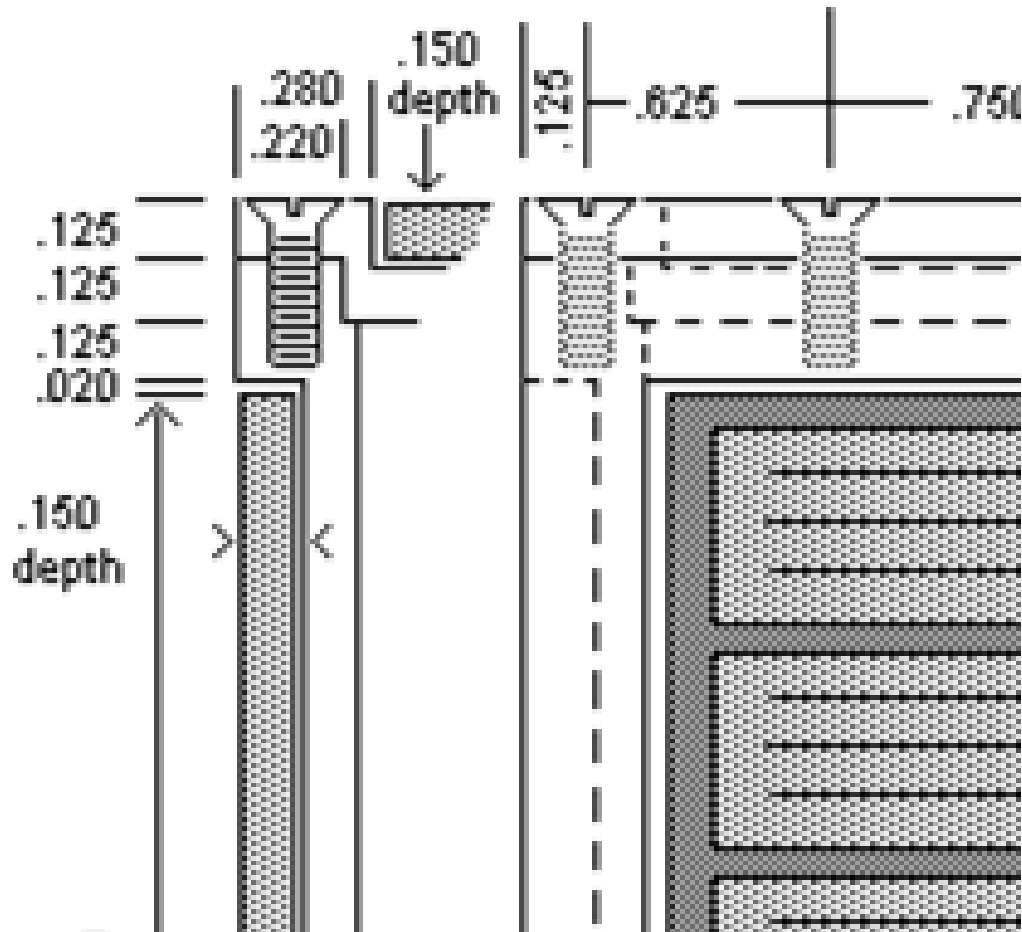
Top Panel



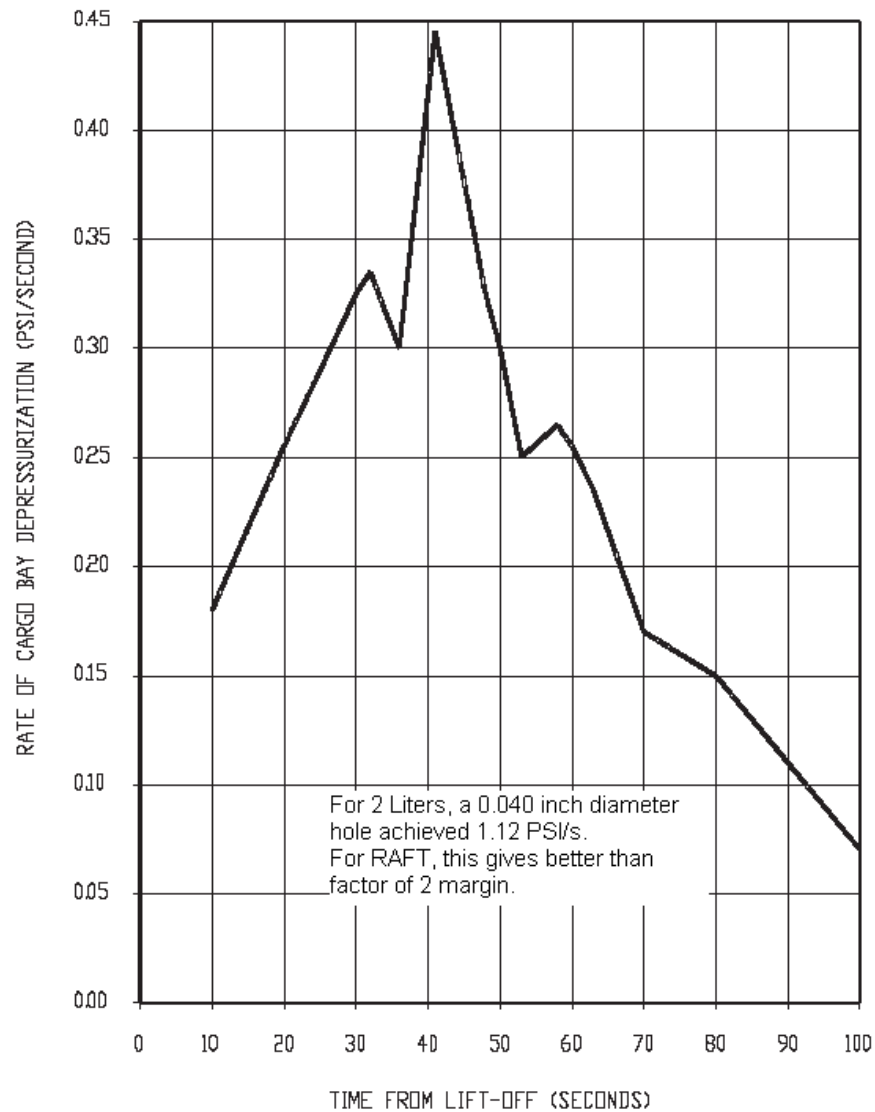
Side Panel



Side Panel Close



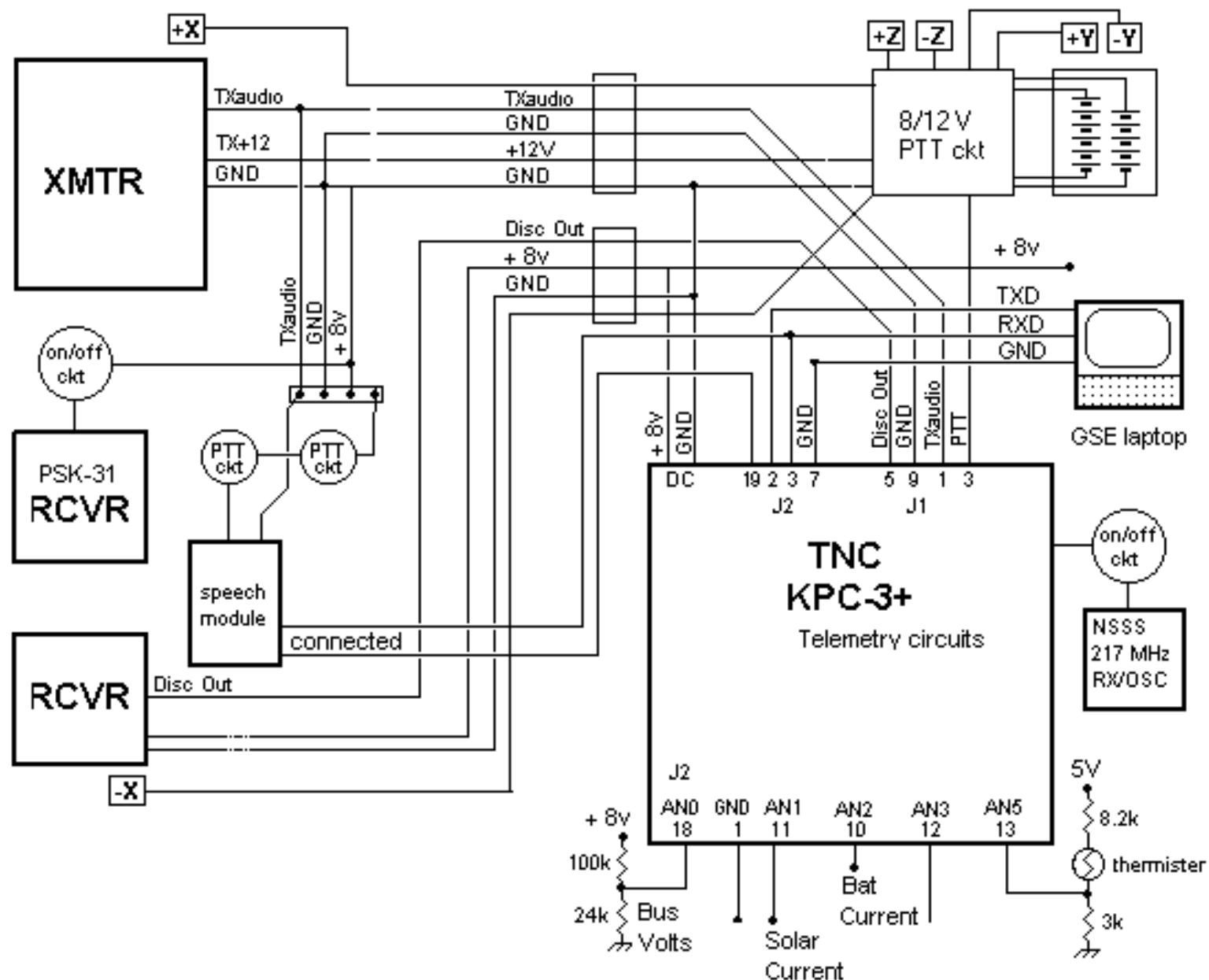
Depressurization Rate



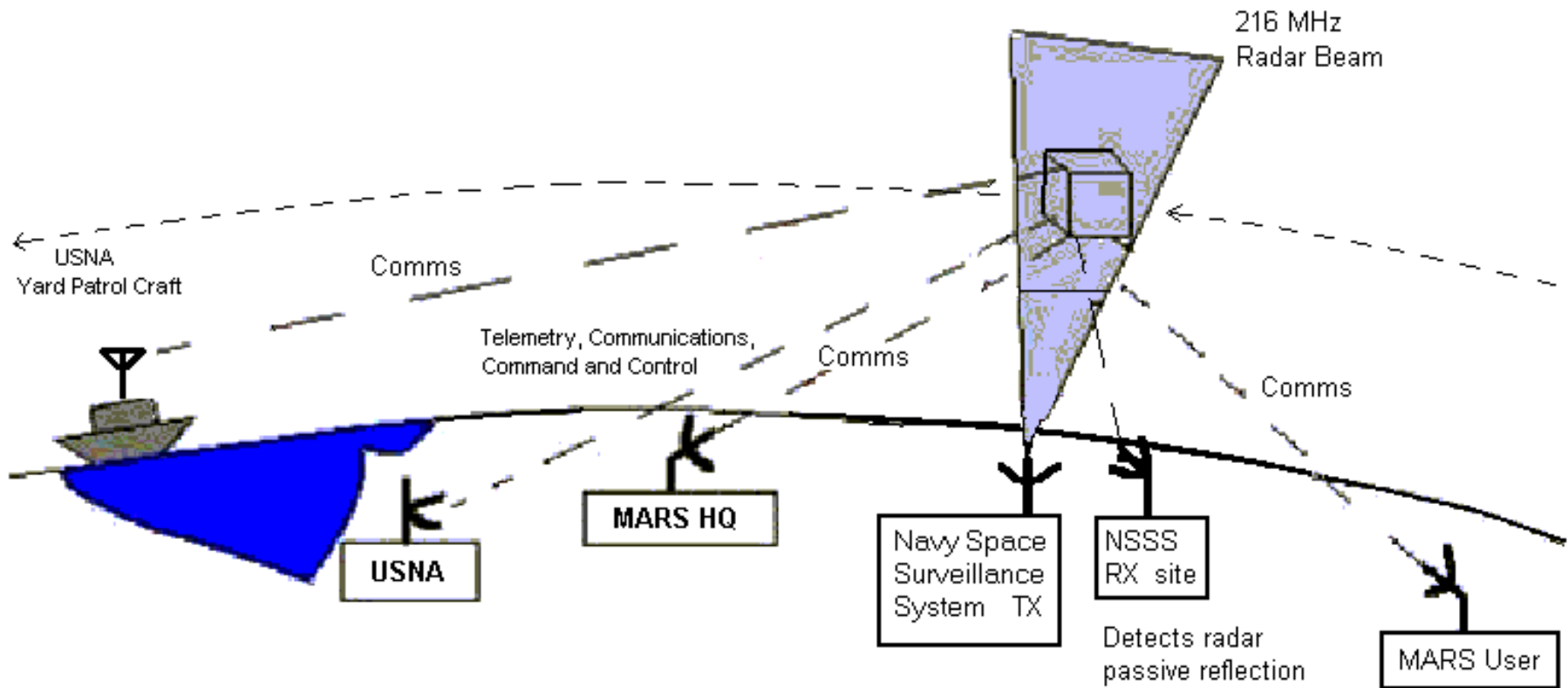
.040 hole
Gives 2:1 margin
for
depressurization

RAFT1 Schematic

PRELIMINARY



MARScom Mission Architecture

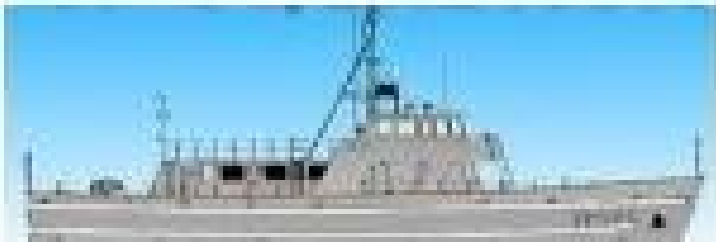


Military Affiliate Radio System

The Mission of the MARS system is to:

- Provide auxiliary communications for military, federal and local disaster management officials during periods of emergency or while conducting drills....
- Assist in effecting normal communications under emergency conditions.
- Handle morale and quasi-official message and voice communications traffic for members of the Armed Forces and authorized U.S. Government civilian personnel
- Provide, during daily routine operations, a method of exchanging MARSGRAMS and ... contacts between service personnel and their families back home.

Yard Patrol Craft Application



The Yard Patrol Craft

105' length

Crew of about 25

Quantity 20



YP COMMS EQUIPMENT

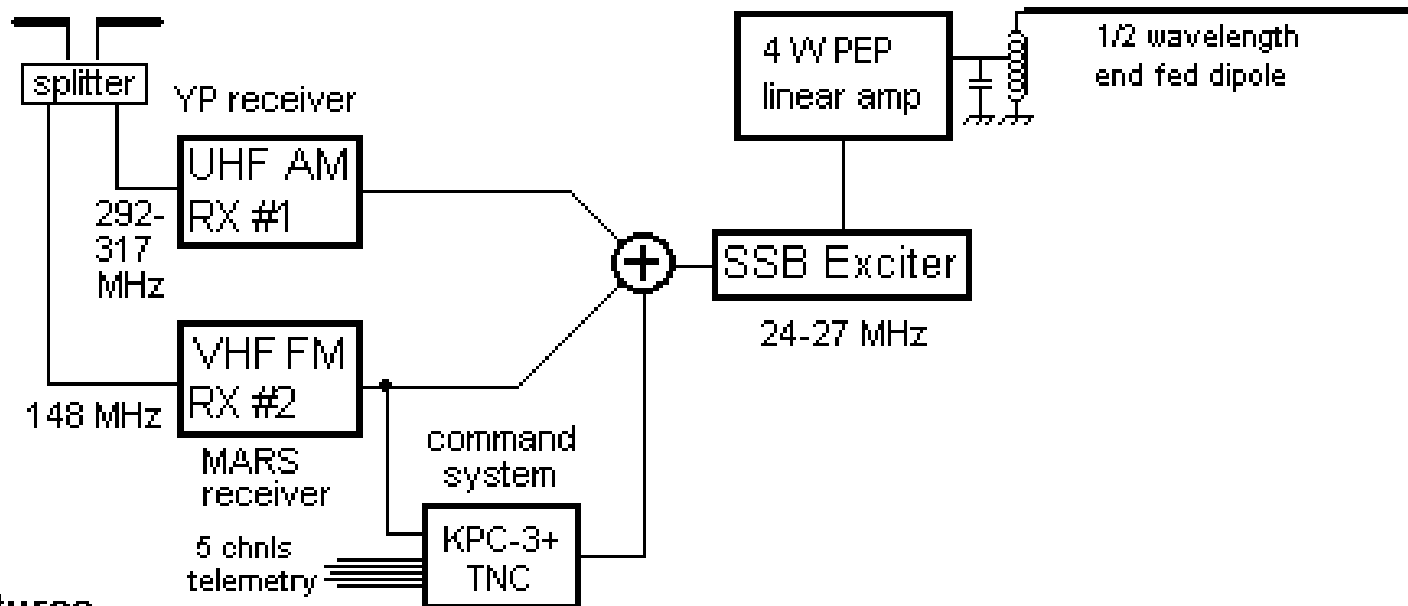
→ Tactical UHF
(uplink)

→ Harris HF Xcvr
(downlink)

MARScom Block Diagram

MARScom Voice Transponder

VHF/UHF dipole



Features

- UHF AM receiver makes MARScom compatible with ALL older UHF transmitters

RAFT Deployment

Velocity of CM:

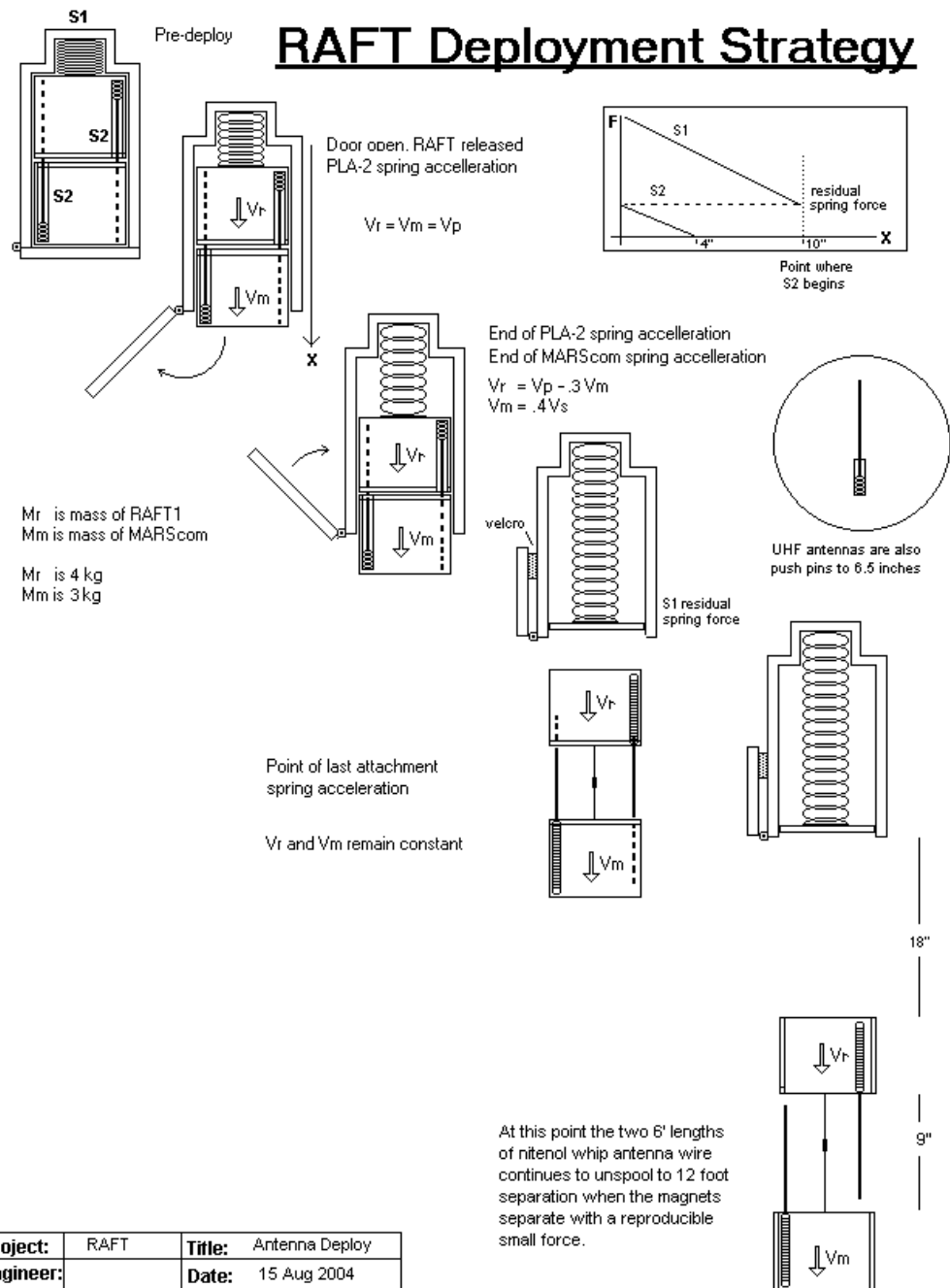
1.00 m/s

Velocity of RAFT:

0.57 m/s

Velocity of MARSCOM:

1.57 m/s



Air Track Separation Test

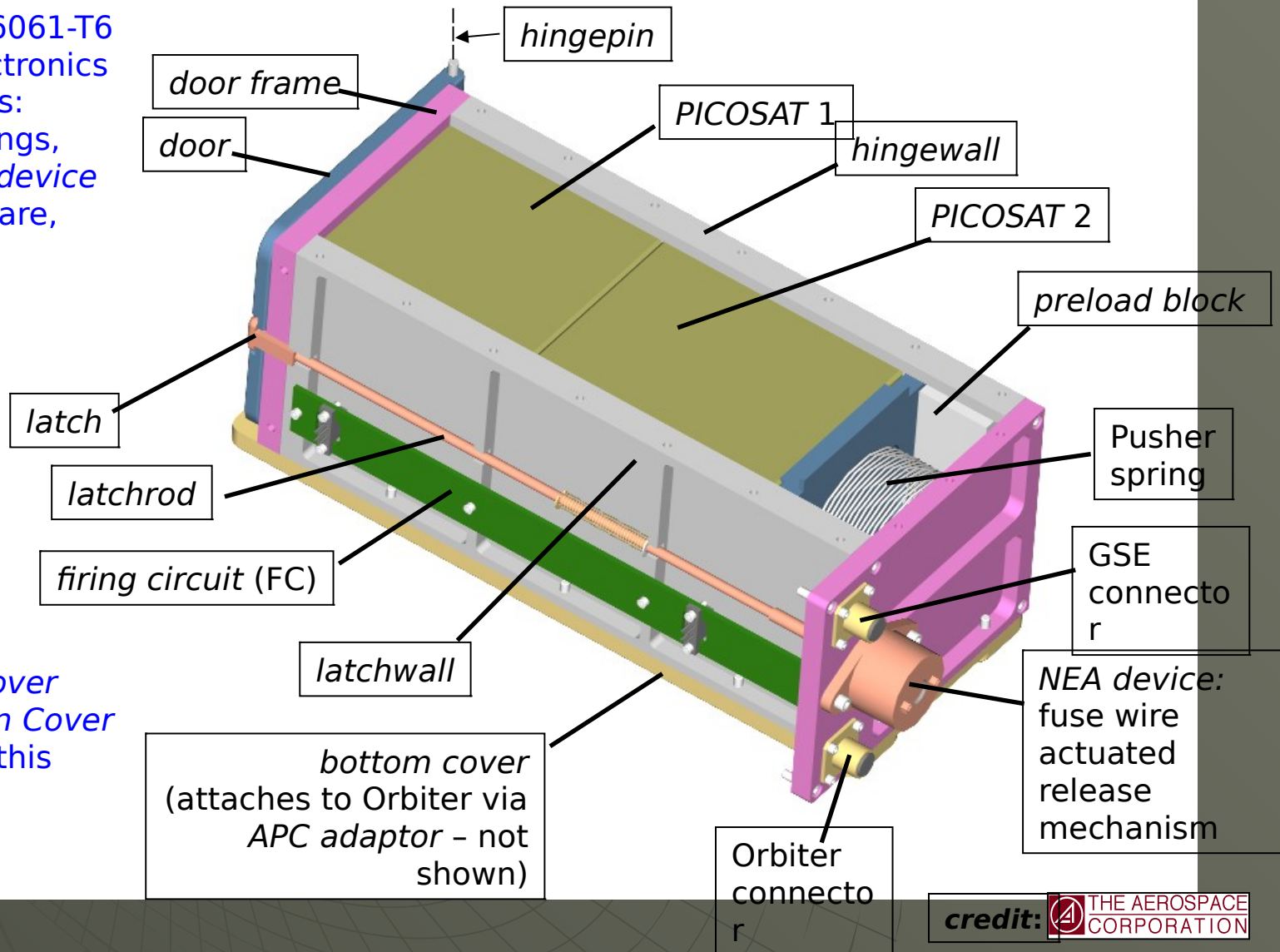


SSPL4410 LAUNCHER: Main Components

MATERIALS:

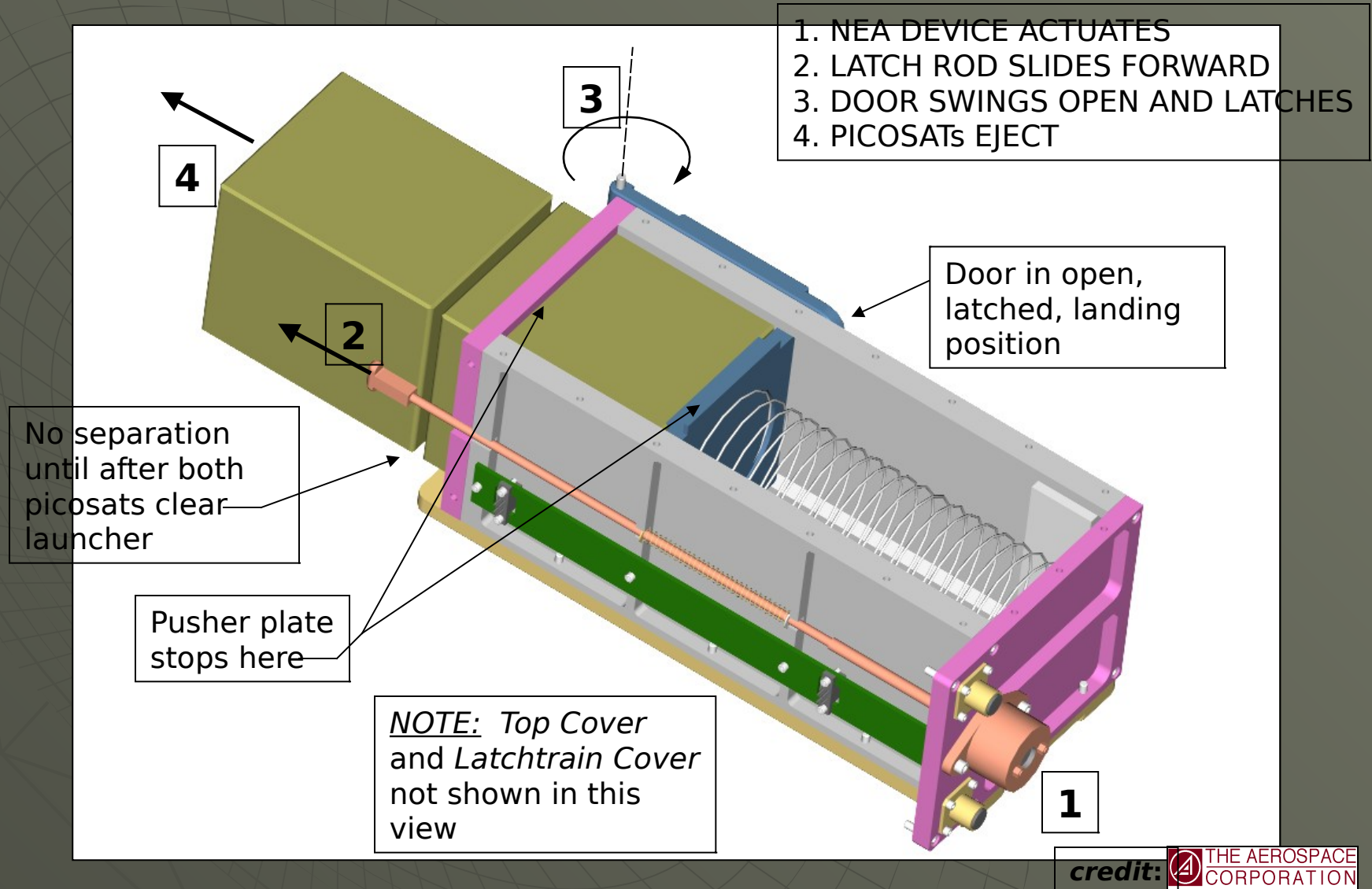
All aluminum 6061-T6
except for electronics
and CRES parts:

fasteners, springs,
latchrod, NEA device
internal hardware,
hingepin



NOTE: Top Cover
and Latchtrain Cover
not shown in this
view

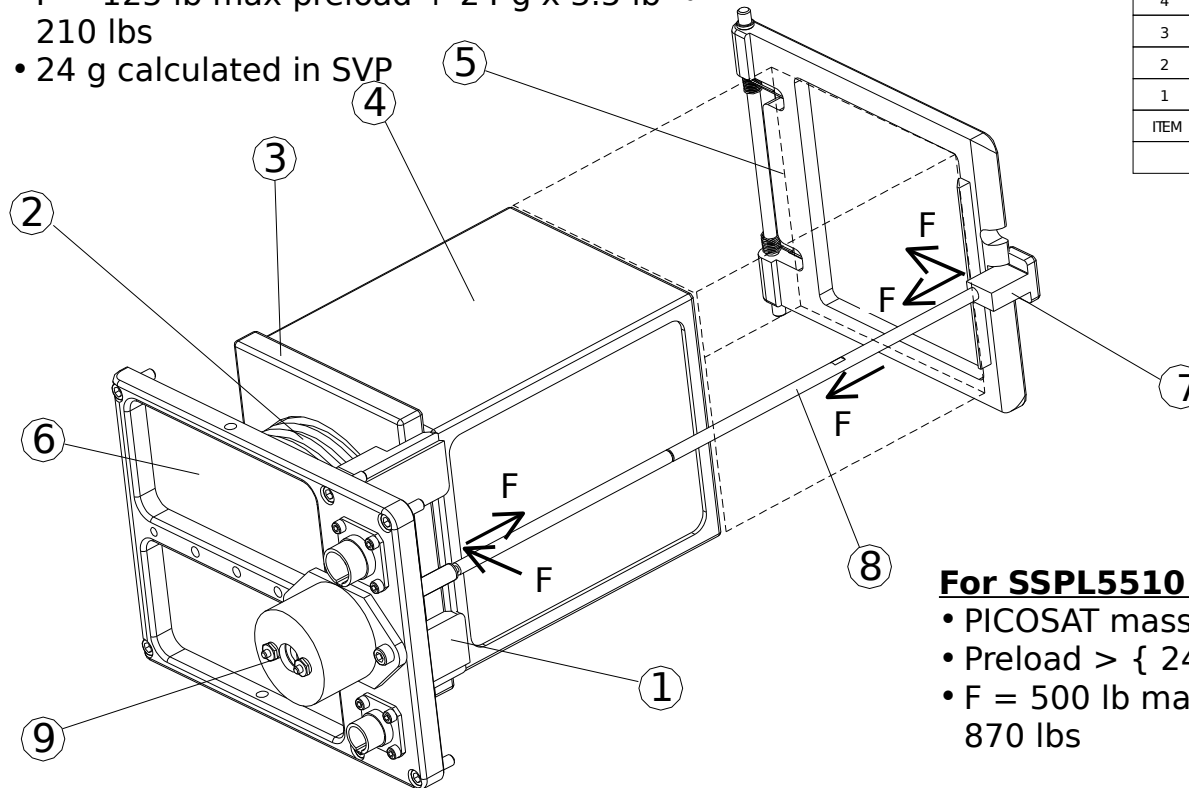
SSPL4410 LAUNCHER: Operation



SSPL4410 LAUNCHER: Preload and Launch Loads

For SSPL4410 with MEPSI:

- PICOSAT mass $m = 1.6 \text{ kg} = 3.5 \text{ lbs}$
- Preload $> \{ 24 \text{ g} \times 3.5 \text{ lbs} = 84 \text{ lbs} \}$
- $F = 125 \text{ lb max preload} + 24 \text{ g} \times 3.5 \text{ lb} \approx 210 \text{ lbs}$
- 24 g calculated in SVP



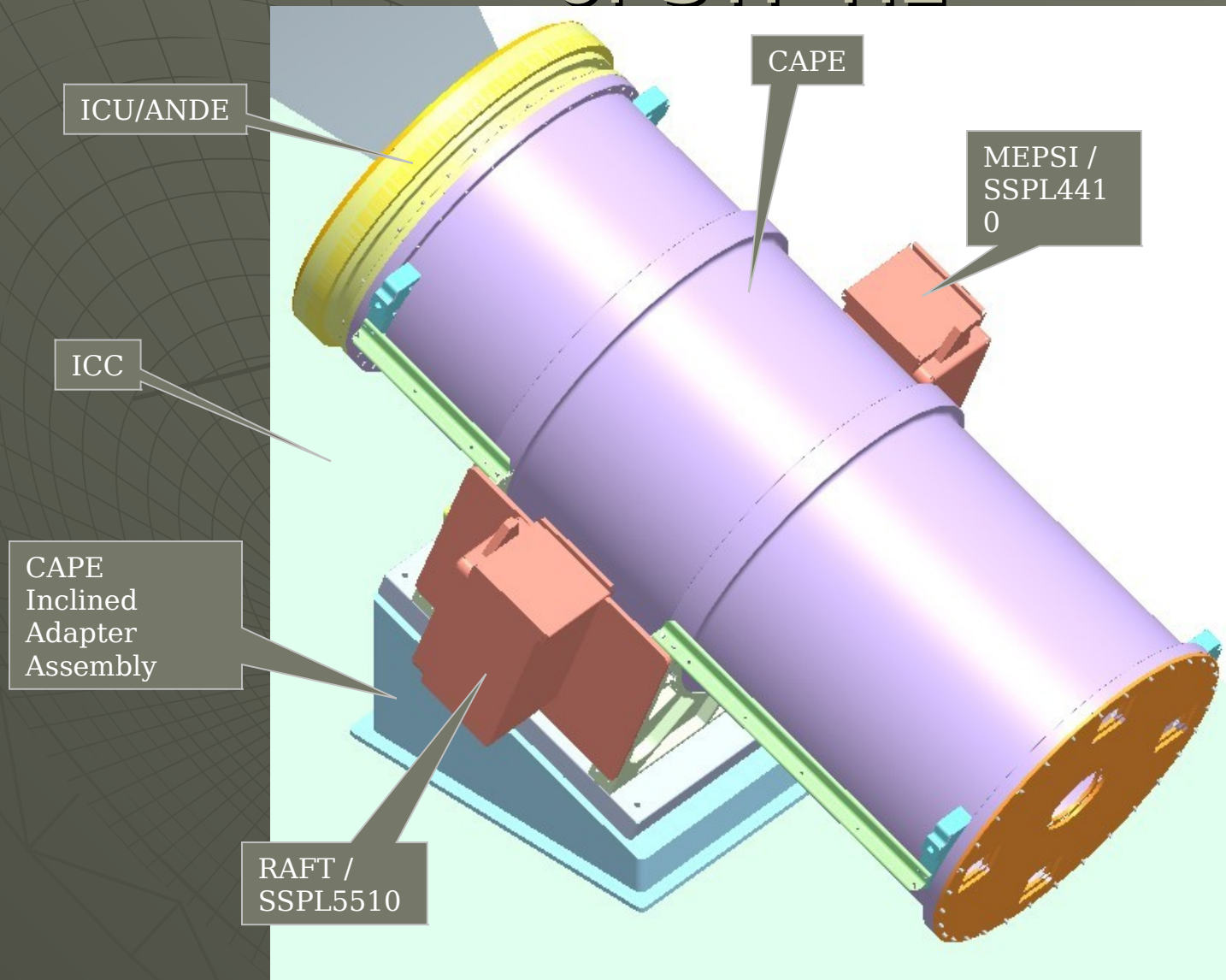
9	1	NEA DEVICE
8	1	LATCH ROD
7	1	LATCH
6	1	BACK COVER
5	1	DOOR
4	2	PICOSAT
3	1	PUSHER
2	1	MAINSRING
1	2	PRELOAD BLOCK
ITEM	QTY	DESCRIPTION
PARTS LIST		

For SSPL5510 with RAFT:

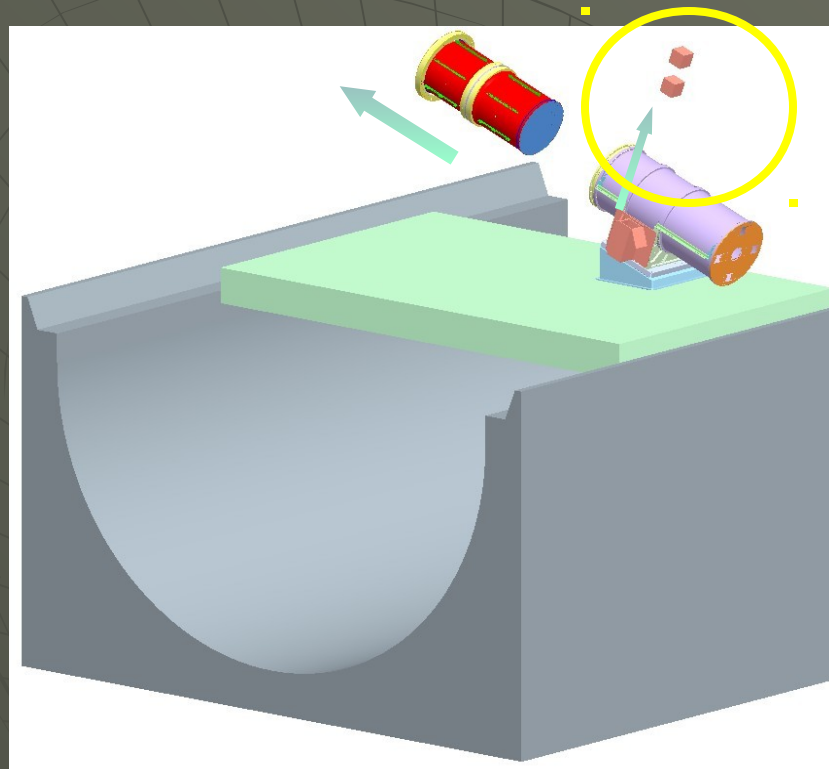
- PICOSAT mass $m = 7 \text{ kg} = 15.4 \text{ lbs}$
- Preload $> \{ 24 \text{ g} \times 15.4 \text{ lbs} = 370 \text{ lbs} \}$
- $F = 500 \text{ lb max preload} + 24 \text{ g} \times 15.4 \text{ lb} \approx 870 \text{ lbs}$

* FRONT PICOSAT NOT SHOWN BUT IS IDENTICAL TO REAR PICOSAT AND REPRESENTED WITH HIDDEN LINES

STS-116 Configuration: RAFT as Part of STP-H2

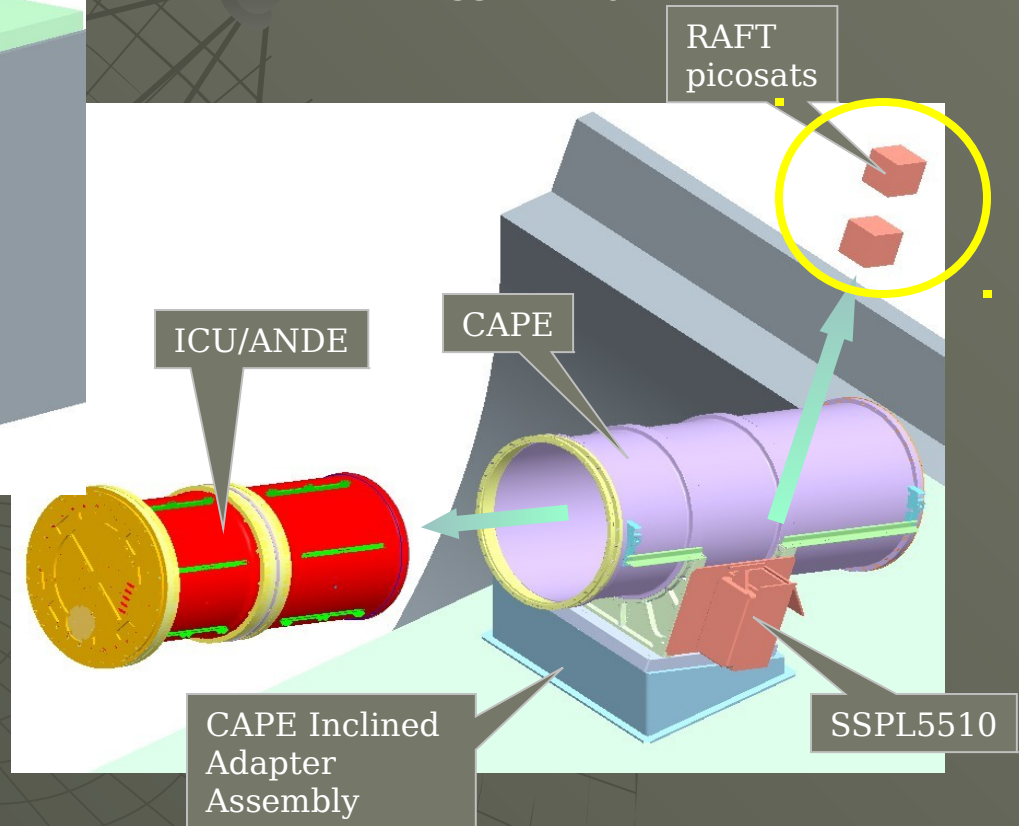


STS-116 Configuration: RAFT as Part of STP-H2



2) *Deployment of RAFT picosats from SSPL5510*

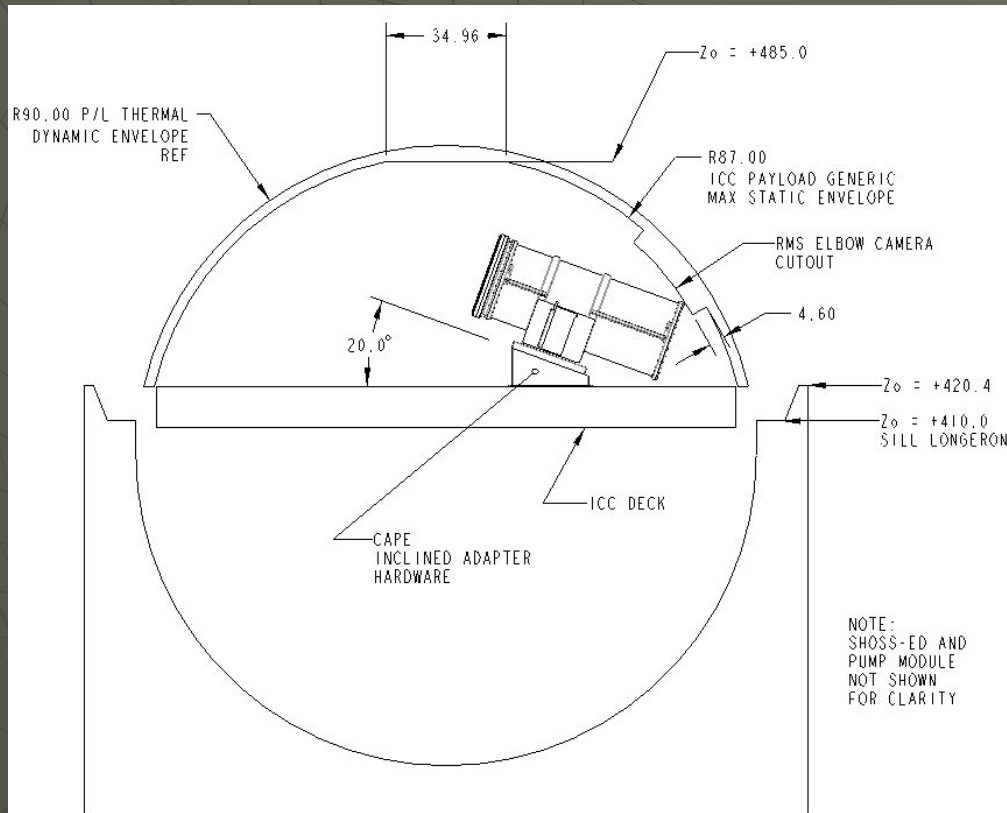
3) *Deployment of MEPSI picosats from SSPL4410*



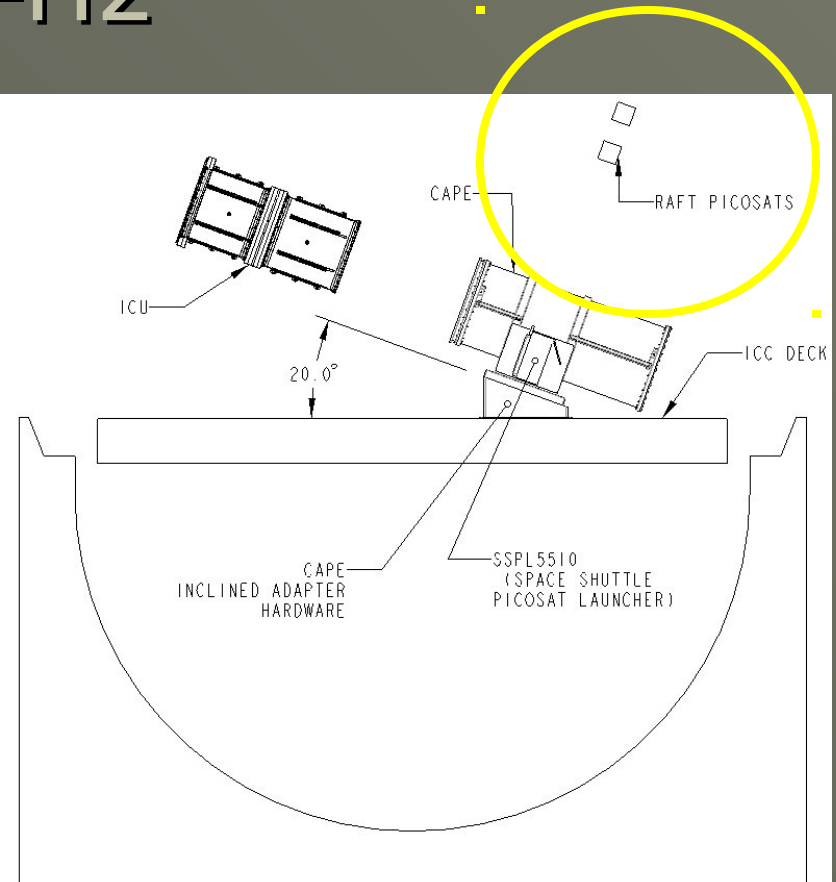
NOTES:

- Non-simultaneous deployment occurs following undock from ISS, not necessarily in the order shown.
- Remaining ICC complement not shown for clarity
- MEPSI/SSPL4410 not shown

STS-116 Configuration: RAFT as Part of STP-H2

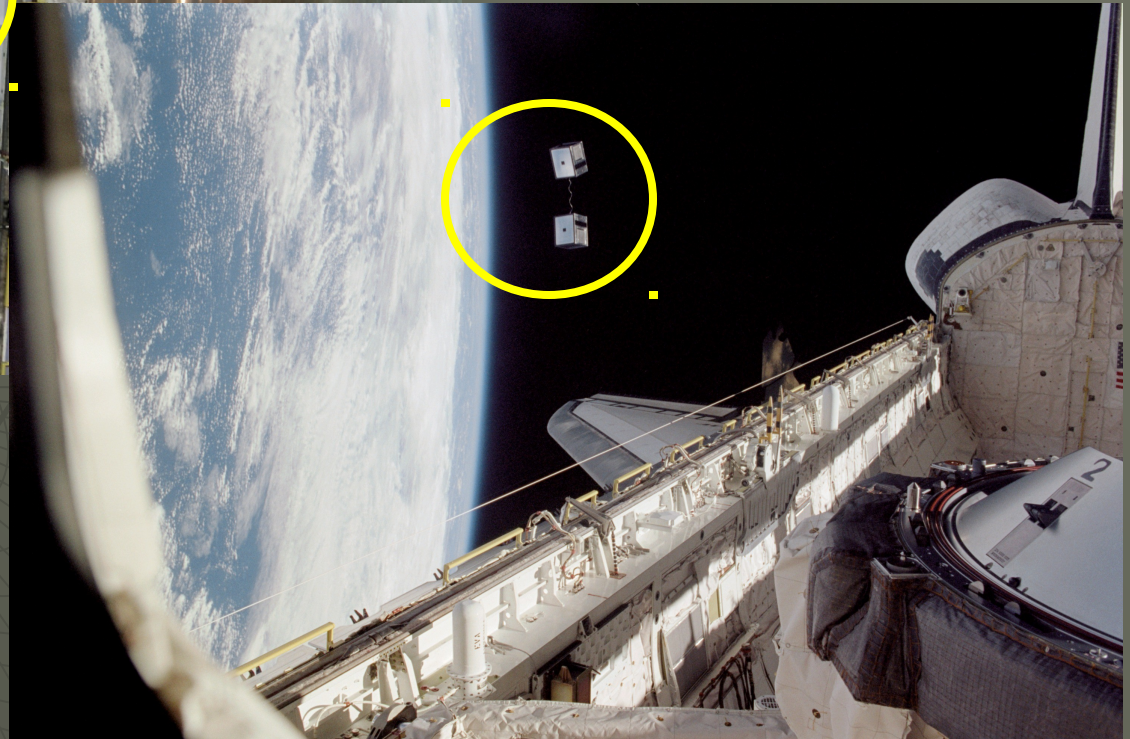
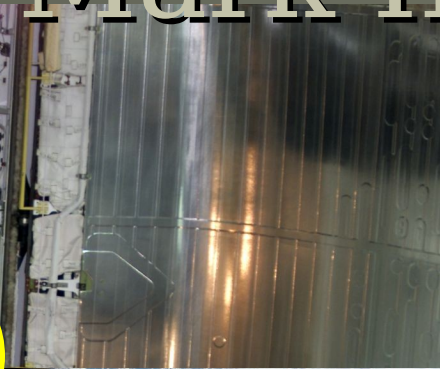
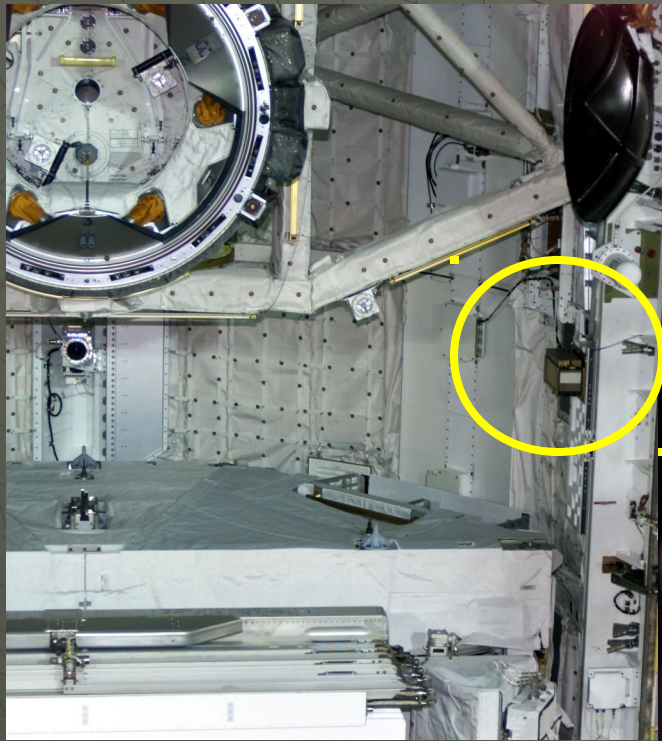


Pre- Deployment

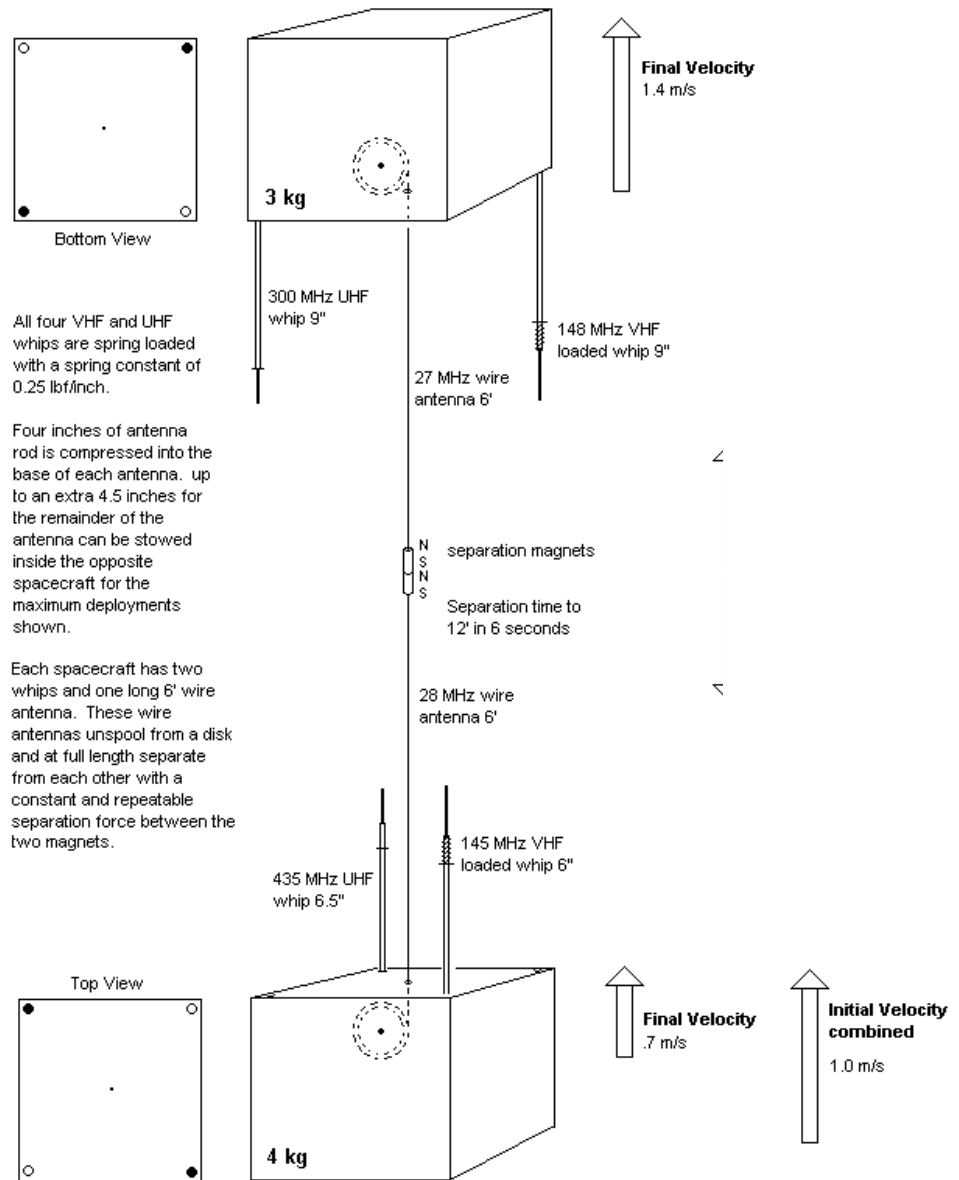


At Deployment

STP PICO Sat Launcher Mark II



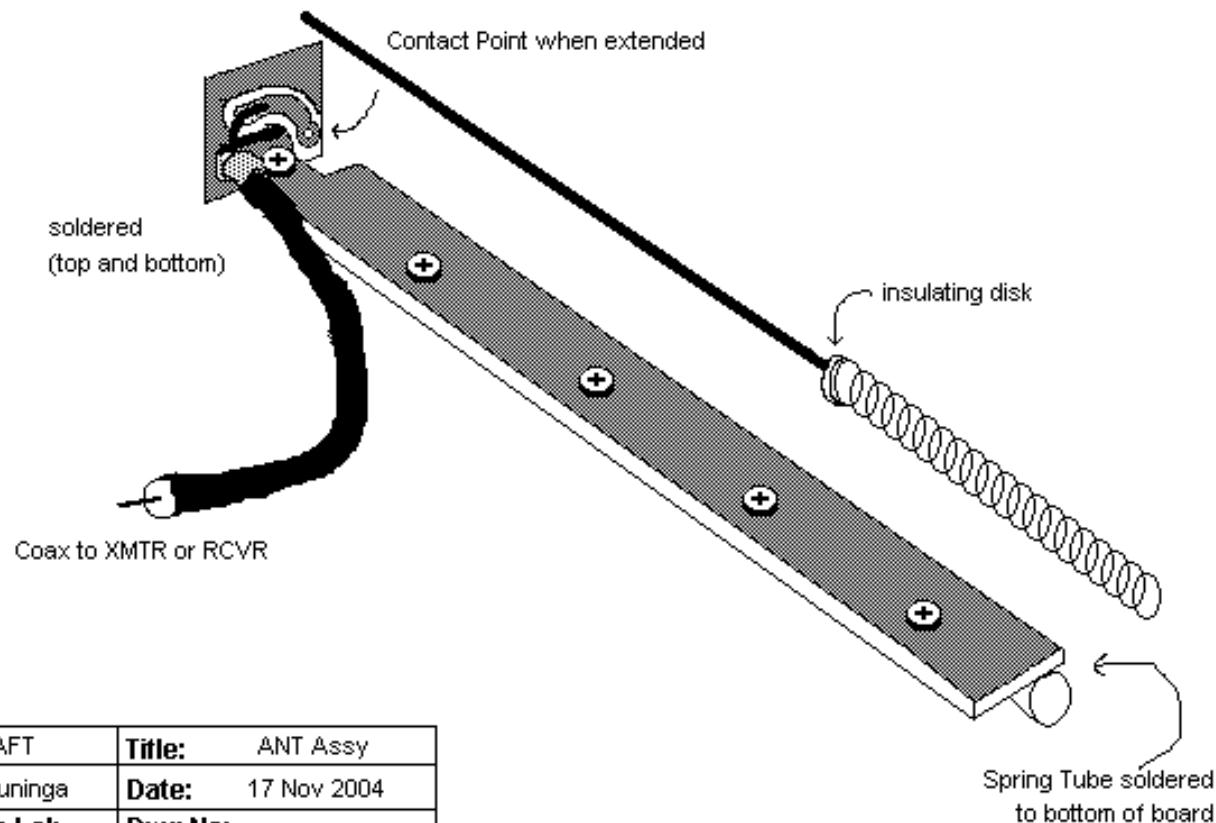
RAFT Antenna Separation Mechanisms



Project:	RAFT	Title:	Simplified Whips
Engineer:	Bruninga	Date:	16 Aug 2004
USNA Satellite Lab	Dwg No:		

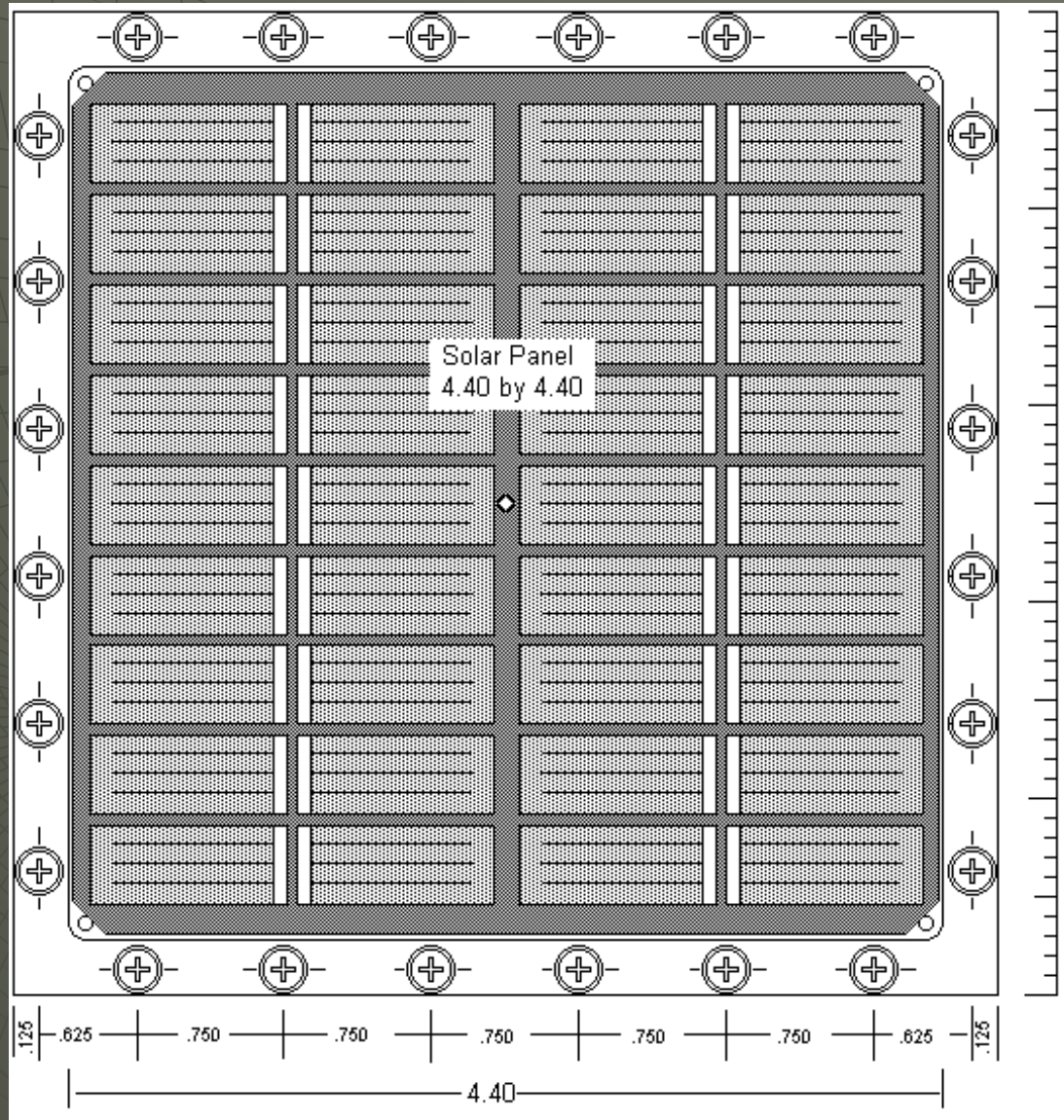
RAFT Antenna Springs

RAFT Spring Antennas and Separation Spring Assembly

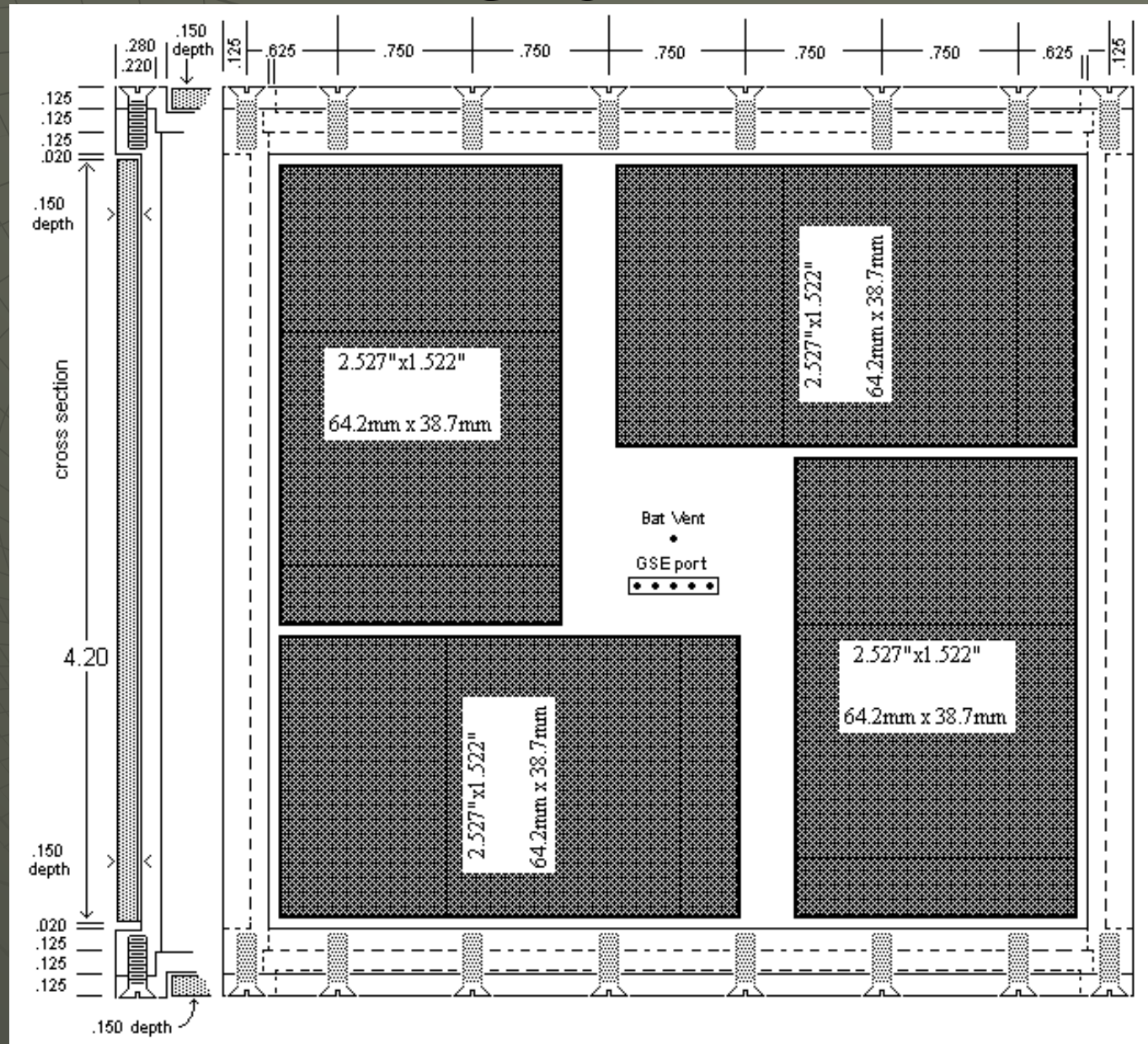


Project:	RAFT	Title:	ANT Assy
Engineer:	Bruninga	Date:	17 Nov 2004
USNA Satellite Lab	Dwg No:		
Web:	http://www.ew.usna.edu/~bruninga/craft/RAFTantASSY2.gif		

Solar Cell Design

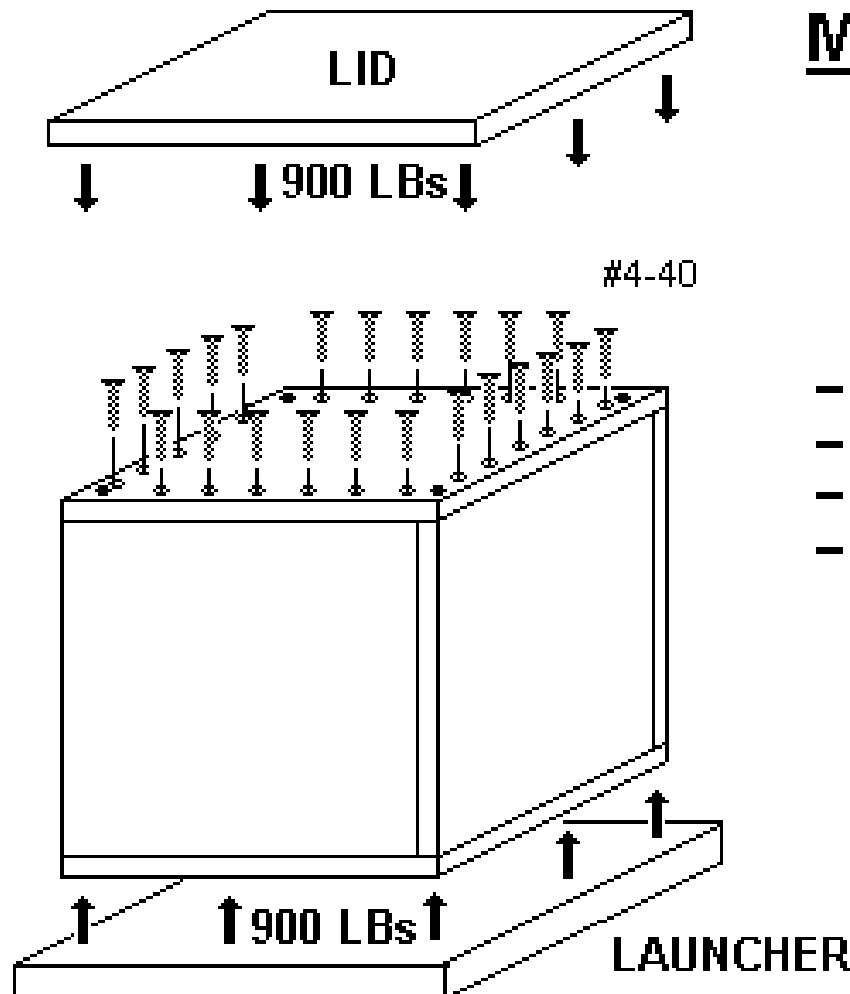


Unique Side Panel for Antenna Crank



Assembly

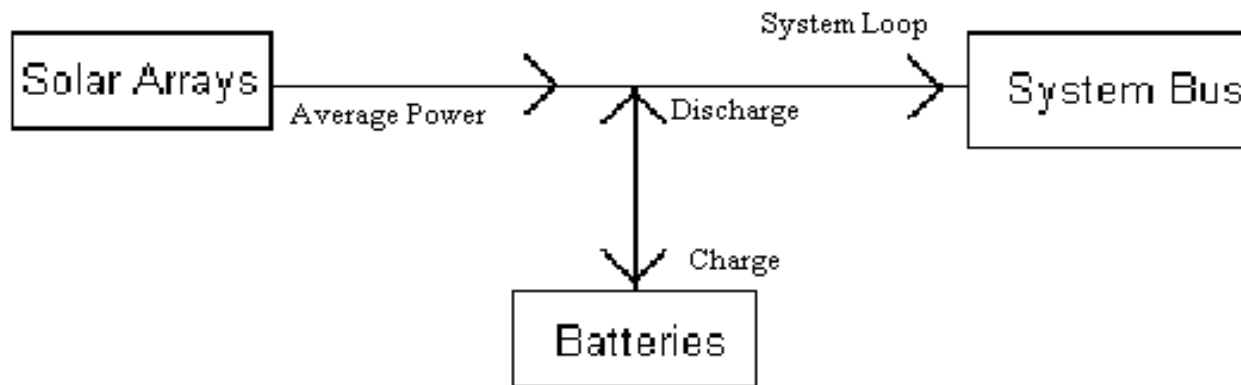
MECHANICAL & FASTENERS



- Four equal 1/4" sides
- Two equal 1/4" Top/Bottoms
- Held under 900 LBs compressive load
- Assures:
 - captive screws
 - no lateral fastener failure modes
 - no Launcher failure modes

Solar Power Budget

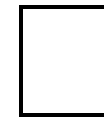
POWER STRUCTURE



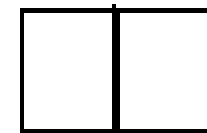
Computing average solar power for a cube satellite taking weighted average of all 26 possible orientations.

This analysis is for an ISS orbit with a maximum eclipse of 39% with a 25% efficient solar cell.

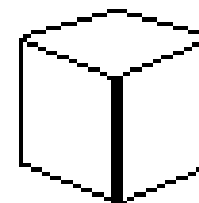
One side in full view
Six Sides



One edge in full view
Twelve edges



One corner in full view
Eight Corners



SC_{eff} =Solar Cell Efficiency	X_e =Eclipse path efficiency
I_d =Elements of Inherent Degradation	L =BusLoad
a =Sun Angle	$P_{BOL} = SC_{eff} * I_d * SolarConstant$
n =number of exposed cells	$P = P_{BOL} * \sin(a)$
A =area of one cell	$P_{totalavg} = P_{avg1} + P_{avg2} + P_{avg3}$
t =exposure multiple	$P_{total} = P * n * A$
t_{total} =total number of exposures	$x = t / t_{total}$
T_d =Time in Daylight	$P_{avg} = P_{total} * x$
T_e =Time in Eclipse	$L = (P_{totalavg} * X_e * X_d * T_d) / (T_e * X_d + T_d * X_e)$
X_d =Daylight path efficiency	

SC_{eff} (%)	25	25	25
I_d	0.77	0.77	0.77
SolarConstant	1367	1367	1367
P_{BOL} (W/m ²)	263.15	263.15	263.15
a (deg)	90	45	33
P (W/m ²)	263.15	186.07	143.32
n	4	8	12
A (m ²)	0.0028	0.0028	0.0028
P_{total} (W)	2.95	4.17	4.82
t	6	12	8
t_{total}	26	26	26
x	1/4	1/2	1/3
P_{avg} (W)	0.6801	1.9237	1.4817
$P_{totalavg}$ (W)	2.08		
T_d	0.61		
T_e	0.39		
X_e	0.65		
X_d	0.85		
L (W)	0.96		

Solar Power Budget

Conclusion:

Using four 25% efficient solar cells per side of the satellite and a 39% eclipse time, an average available bus load of 0.96 watts will be available to the spacecraft

RAFT1 Required Power Budget

	Current (mA)	Normal	Avg (mA)	PSK-31	Avg (mA)	STBY	Avg (mA)
VHF FM TX	500.00	2%	10.00	10%	50.00	1%	5.00
UHF FM RX	30.00	100%	30.00	100%	30.00	100%	30.00
TNC	15.00	100%	15.00	100%	15.00	100%	15.00
Down Converter	50.00	0%	0.00	10%	0.05	0%	0.00
29 MHz RX	50.00	0%	0.00	10%	0.05	0%	0.00
20% Reserve	9.00		9.00		9.00		9.00
Avg (mA)			64.00			104.10	59.00

	Normal Use	PSK-31	STBY	Available
Avg(mA)	64.00	104.10	59.00	114.2857
System (Volts)	8.40	8.40	8.40	8.4
Avg (Watts)	0.5376	0.87444	0.4956	0.96

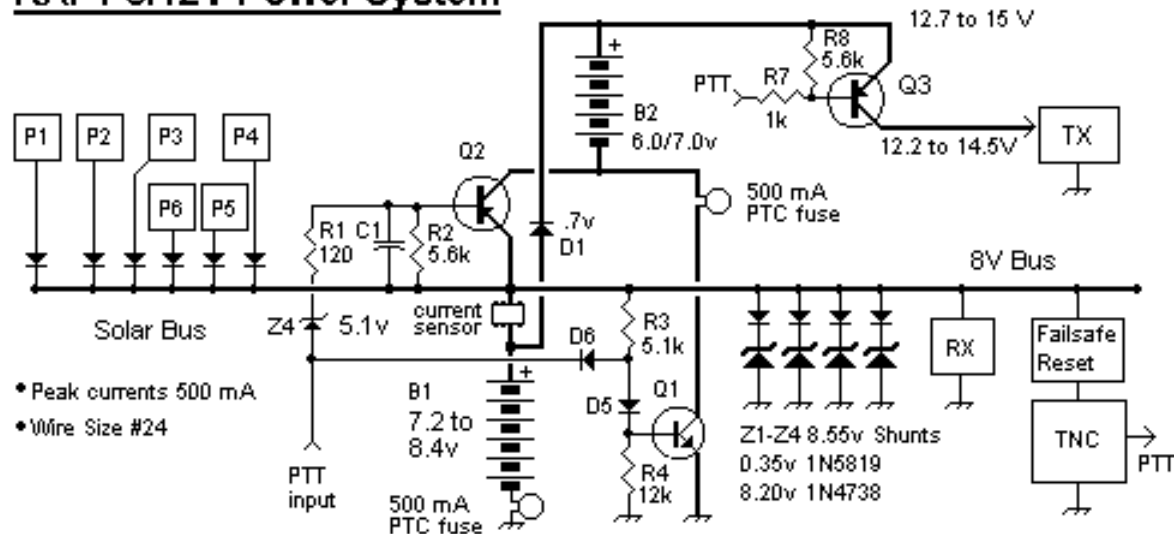
MARScom Required Power Budget

	Current (mA)	Normal	Current (mA)	YPSATCOM	Current (mA)
VHF FM RX	30.00	100%	30.00	100%	30.00
UHF AM RX	30.00	0%	0.00	100%	30.00
SSB Exciter	50.00	8.34%	4.17	8.34%	4.17
1W Linear PA	100.00	8.34%	8.34	8.34%	8.34
Decoder	10.00	100%	10.00	100%	10.00
20% Reserve	8.00		8.00		8.00
Avg (mA)			60.51		90.51

	Normal Use	YPSATCOM	Available
Avg (mA)	60.51	90.51	114.2857143
System (Volts)	8.40	8.40	8.4
Avg (Watts)	0.51	0.76	0.96

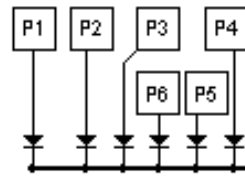
Power System

RAFT 8/12V Power System



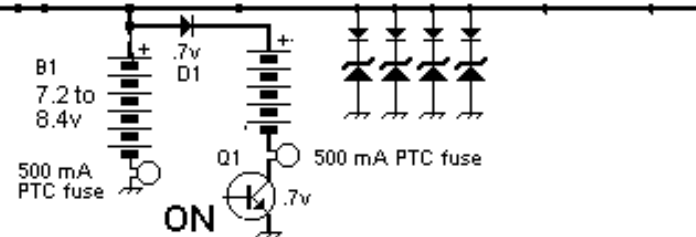
- Battery B1 is 6 cells NiCd feeding 7.2-8.4 unregulated bus to the TNC and Receiver.
- Solar panels provide about 250 mA at 8.5 volts to charge B1 and B2 in parallel via D1 and Q1.
- Q1 is saturated on via R3/D5 during charge. When PTT goes low, D6 pulls Q1 base to OFF via R4
- Excess solar power above 8.55V is shunted via Z1-Z4 leaving about 25 mA to each string
- Z4/R1 and R7 turn ON Q2 and Q3 connecting B1/B2 in series to provide 12 to 14.2 volts to the XMTR.
- The R1-C1 time constant and Zener Z4 assures that both Q1 and Q2 will not be on at the same time.
- Charging efficiency is 91% of normal, discharge efficiency is 98% of normal.

Simplified Power System

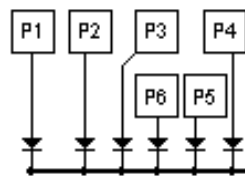


Parallel Charge

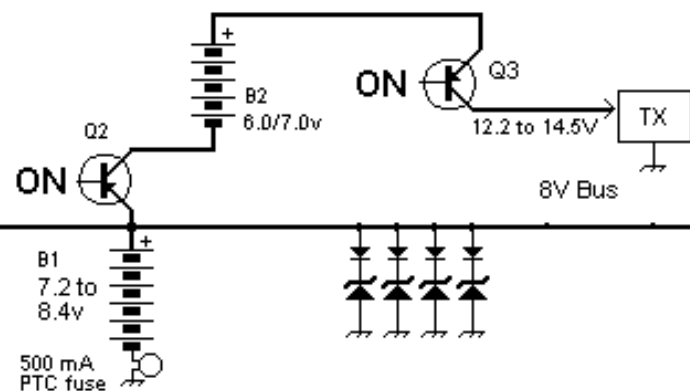
Note: The 0.7V drops across D1 and Q1 equals the 1.4 Volt drop across the missing cell so no cross charging is normally possible. If a cell fails short then cross charge current is limited by Q1 acting in a constant current mode. Current is limited to 0.2C.



See Charge Safety Document: <http://www.ew.usna.edu/~bruninga/craft/RAFTchargeSafety.txt>



Series Transmit

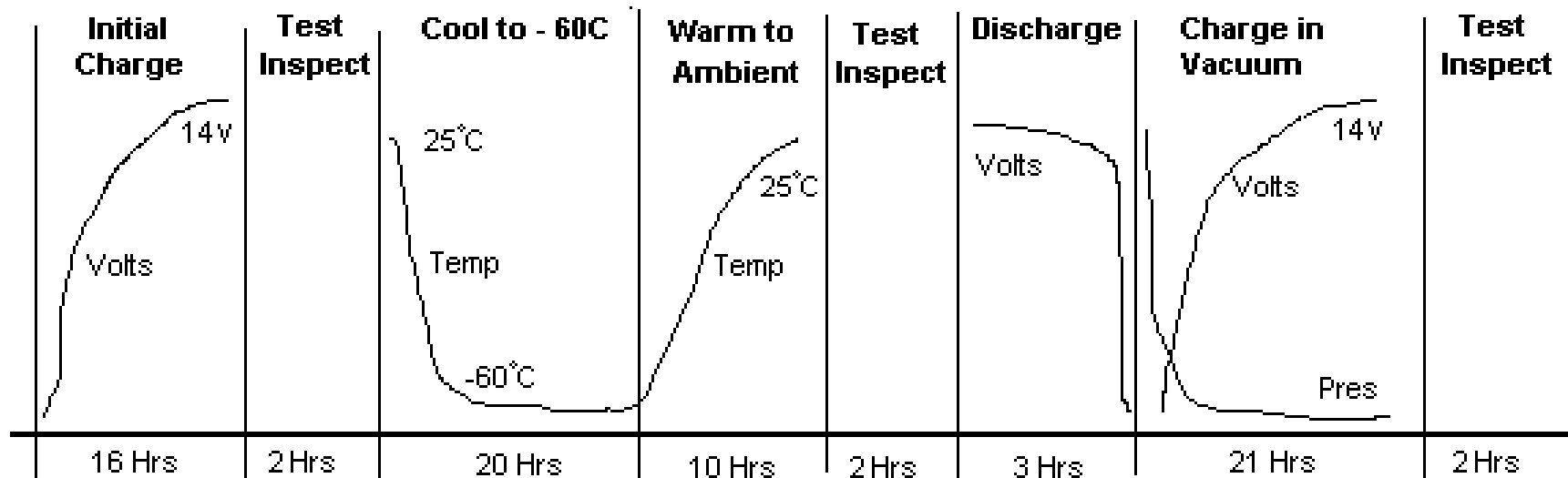


-60 °C Battery Tests

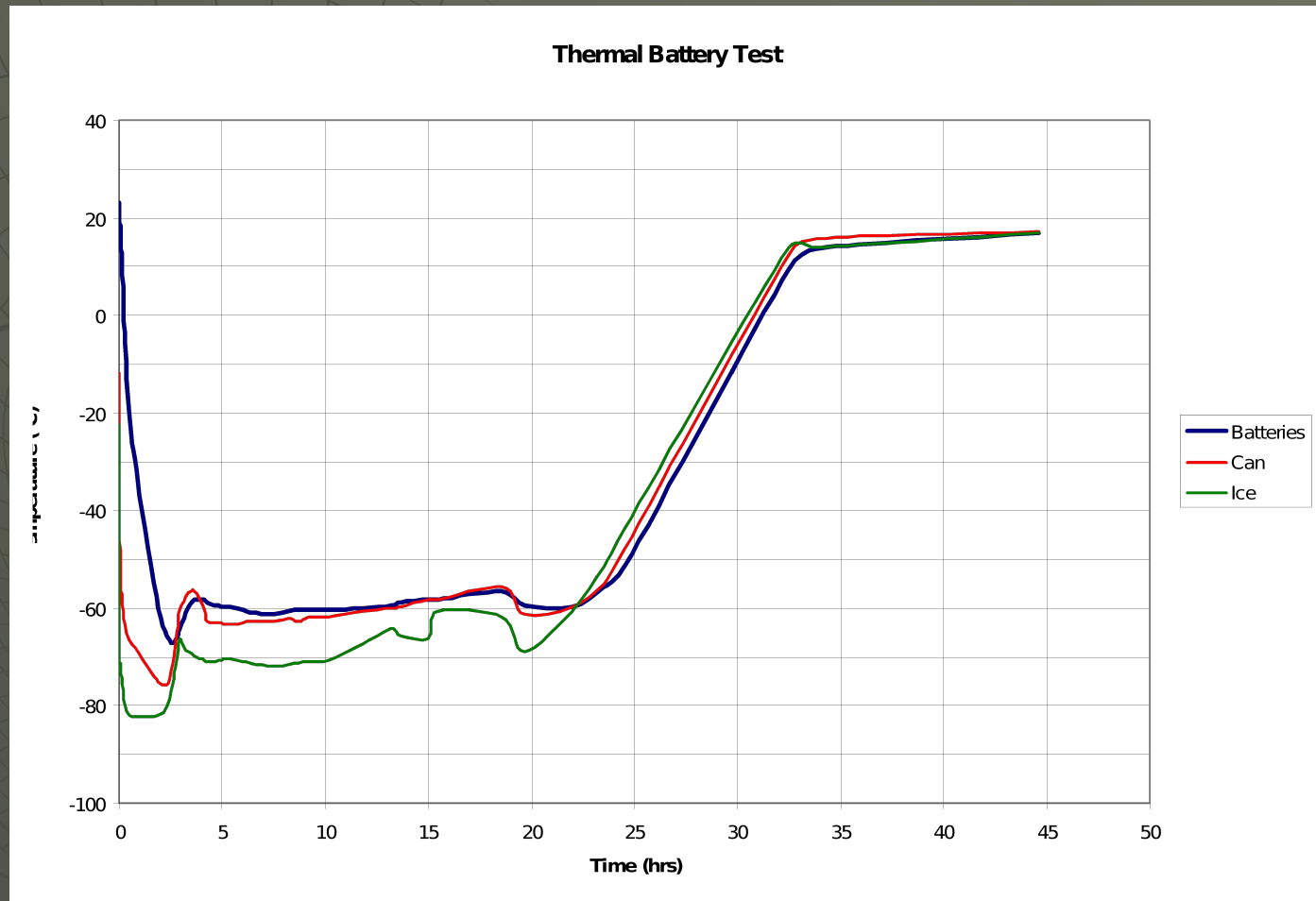


Time Line

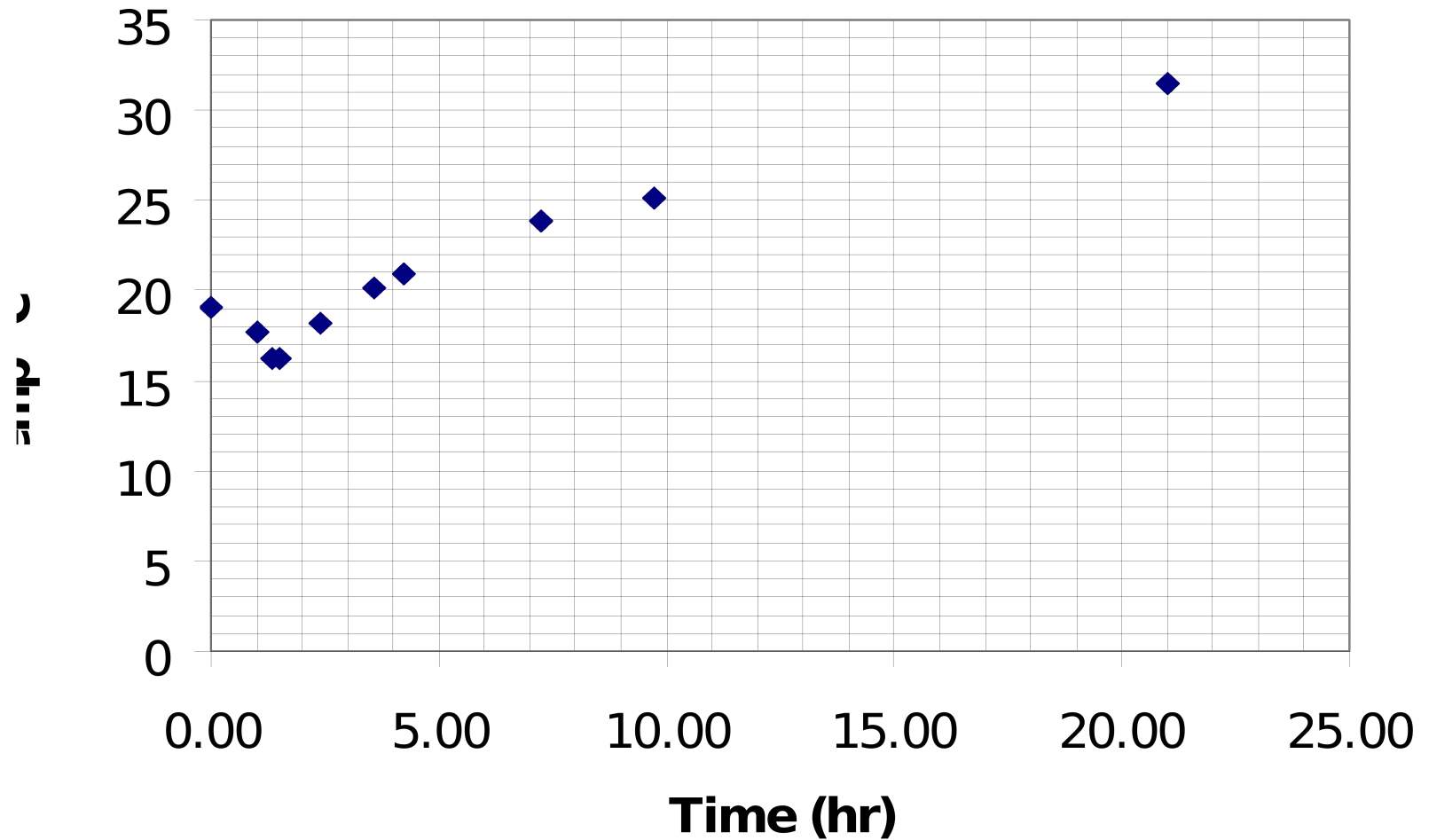
Battery Cold Test Time Line (-60 C)



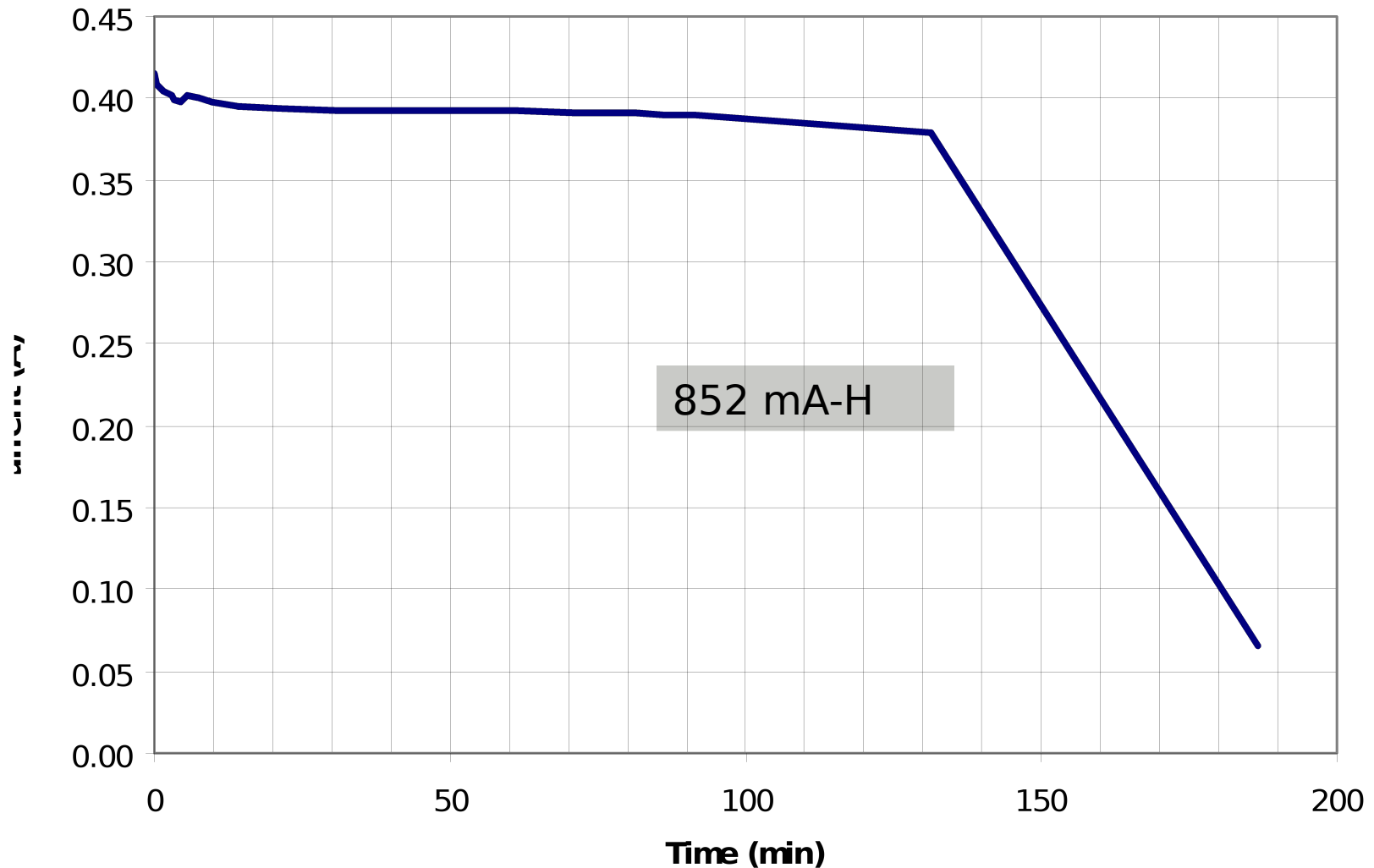
-60 °C Battery Test: Thermal Conditions



-60 °C Battery Test: Charge Temp



Post Cold Test Discharge Current

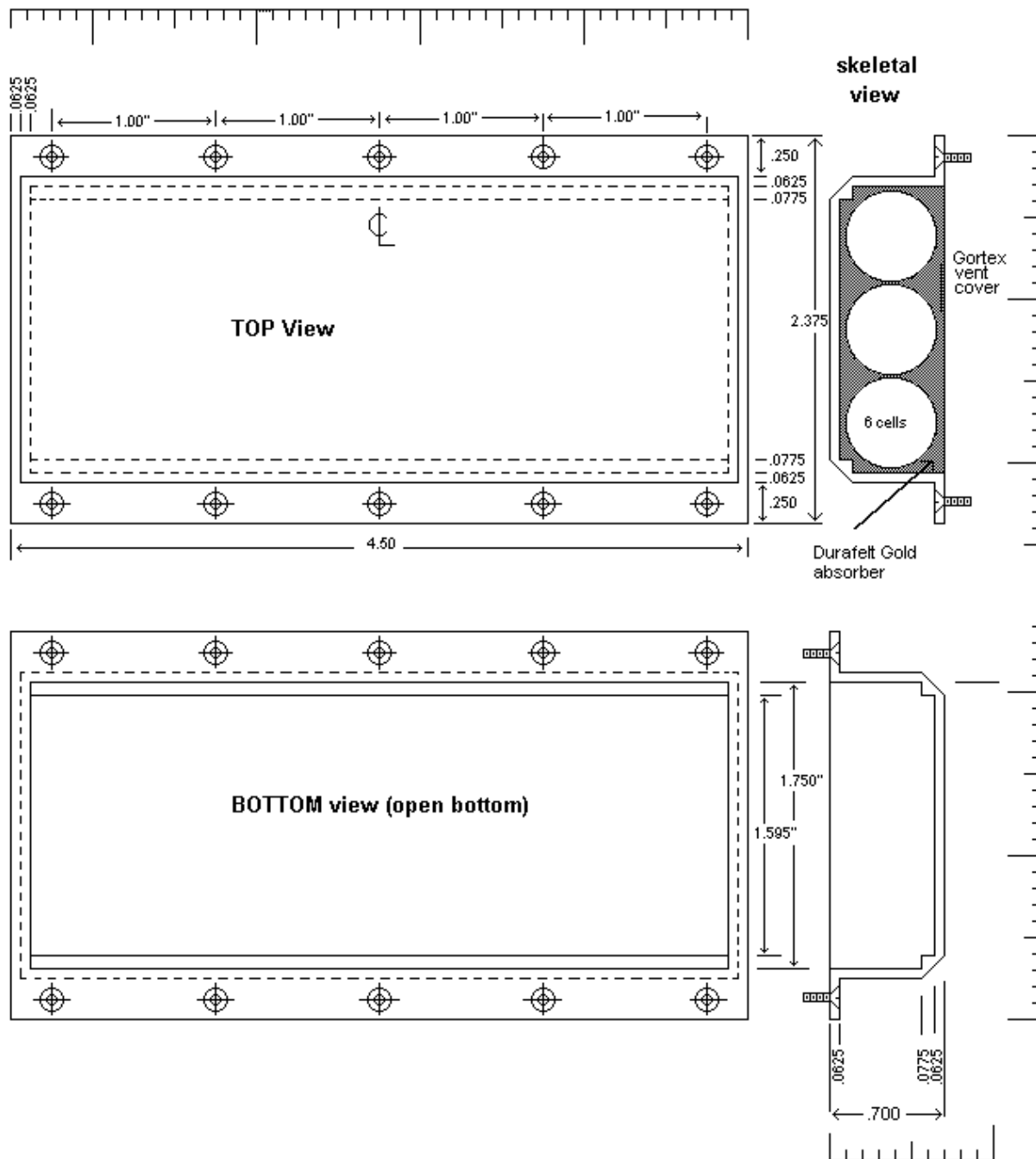


Post Cold Test Battery Condition (No Leakage)

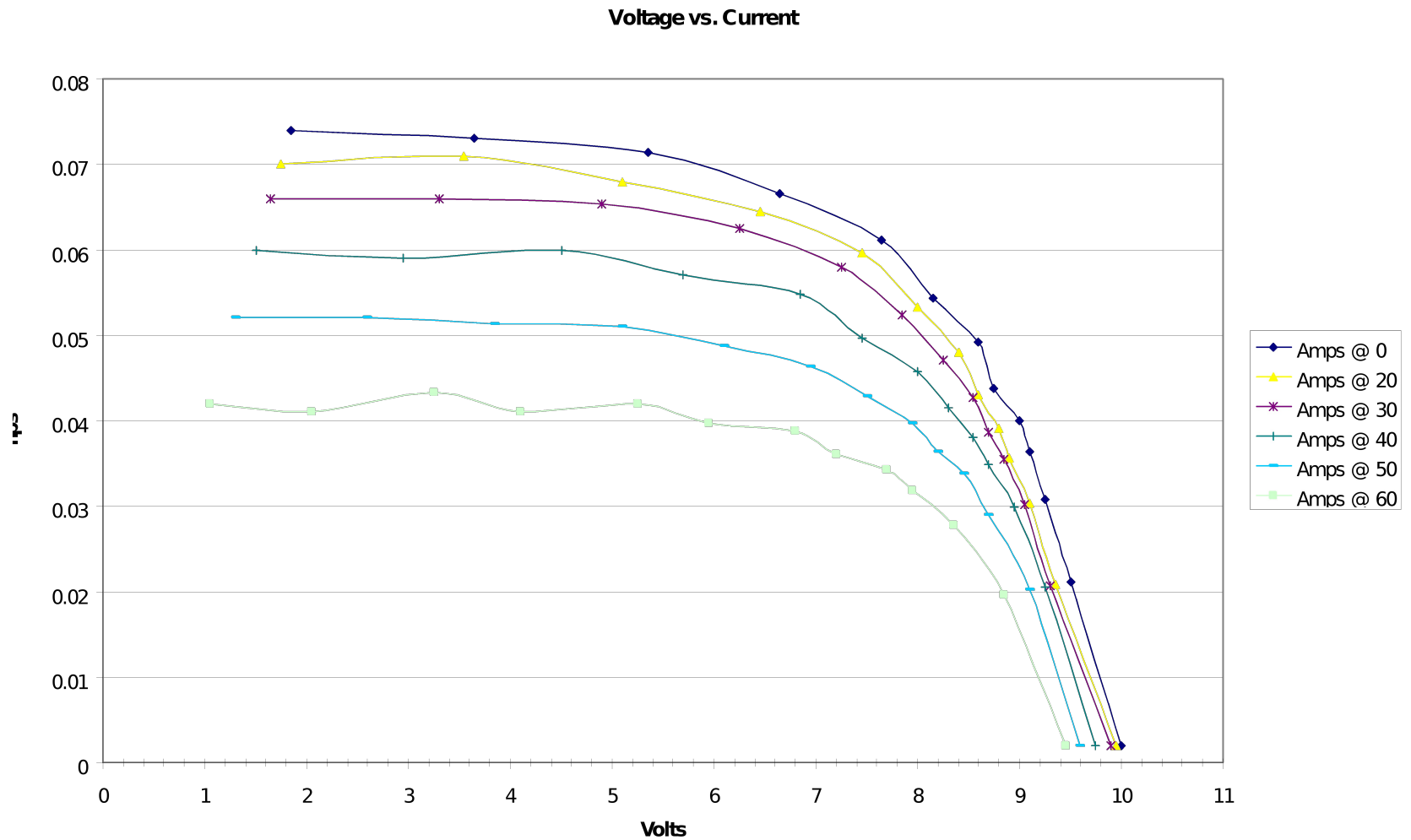


No leakage detected

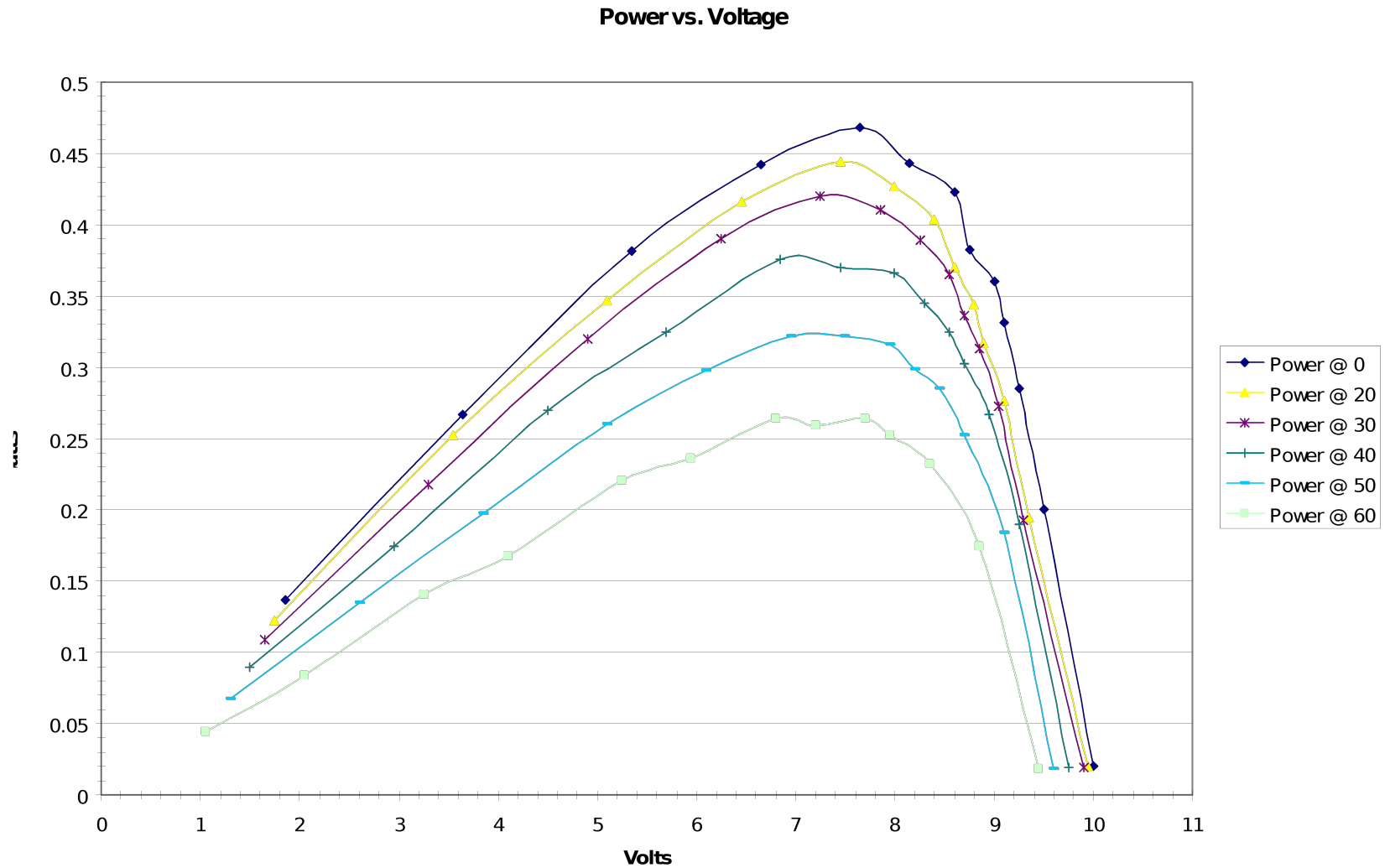
Battery Box



PCsat I-V Curve



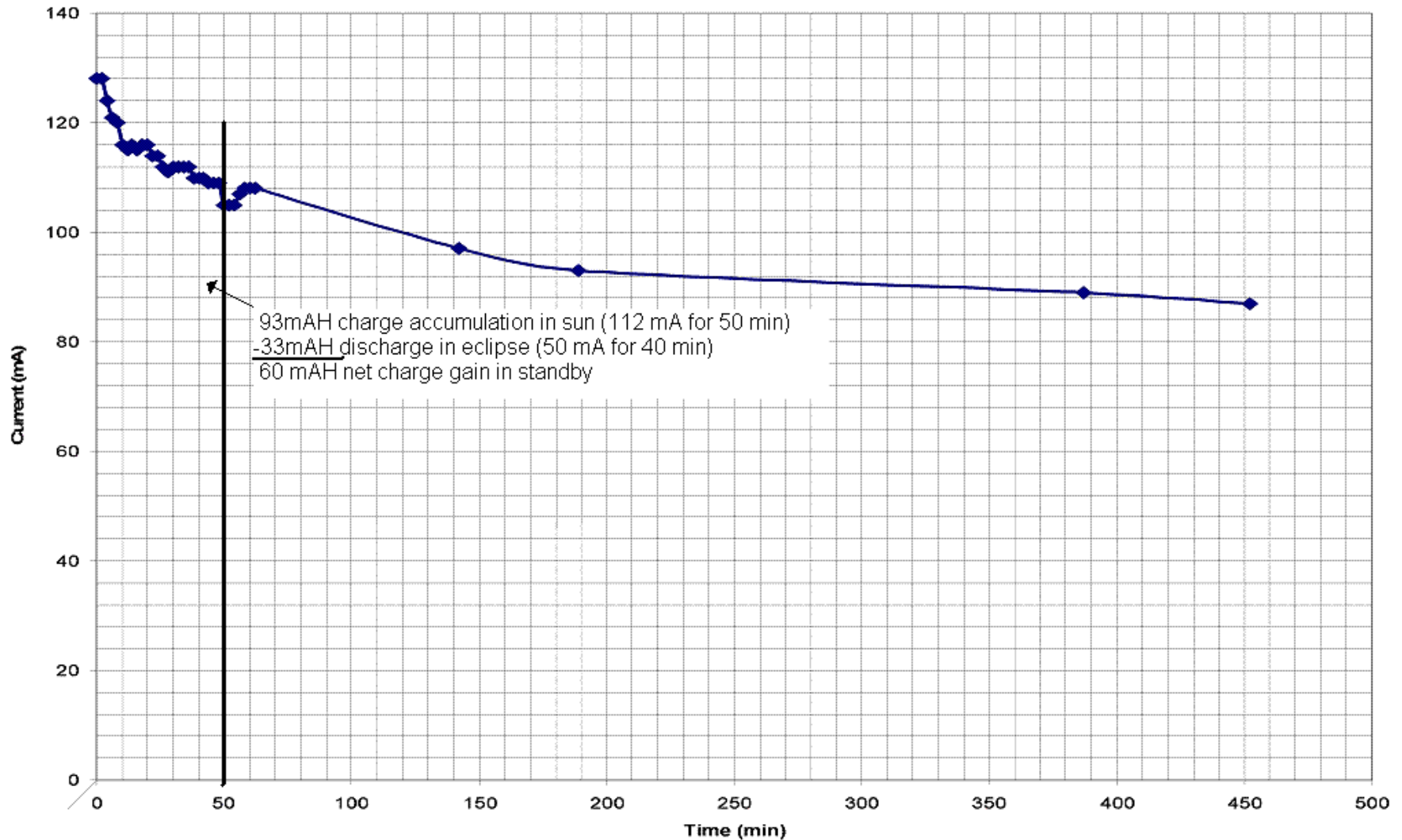
PCsat P-V Curve



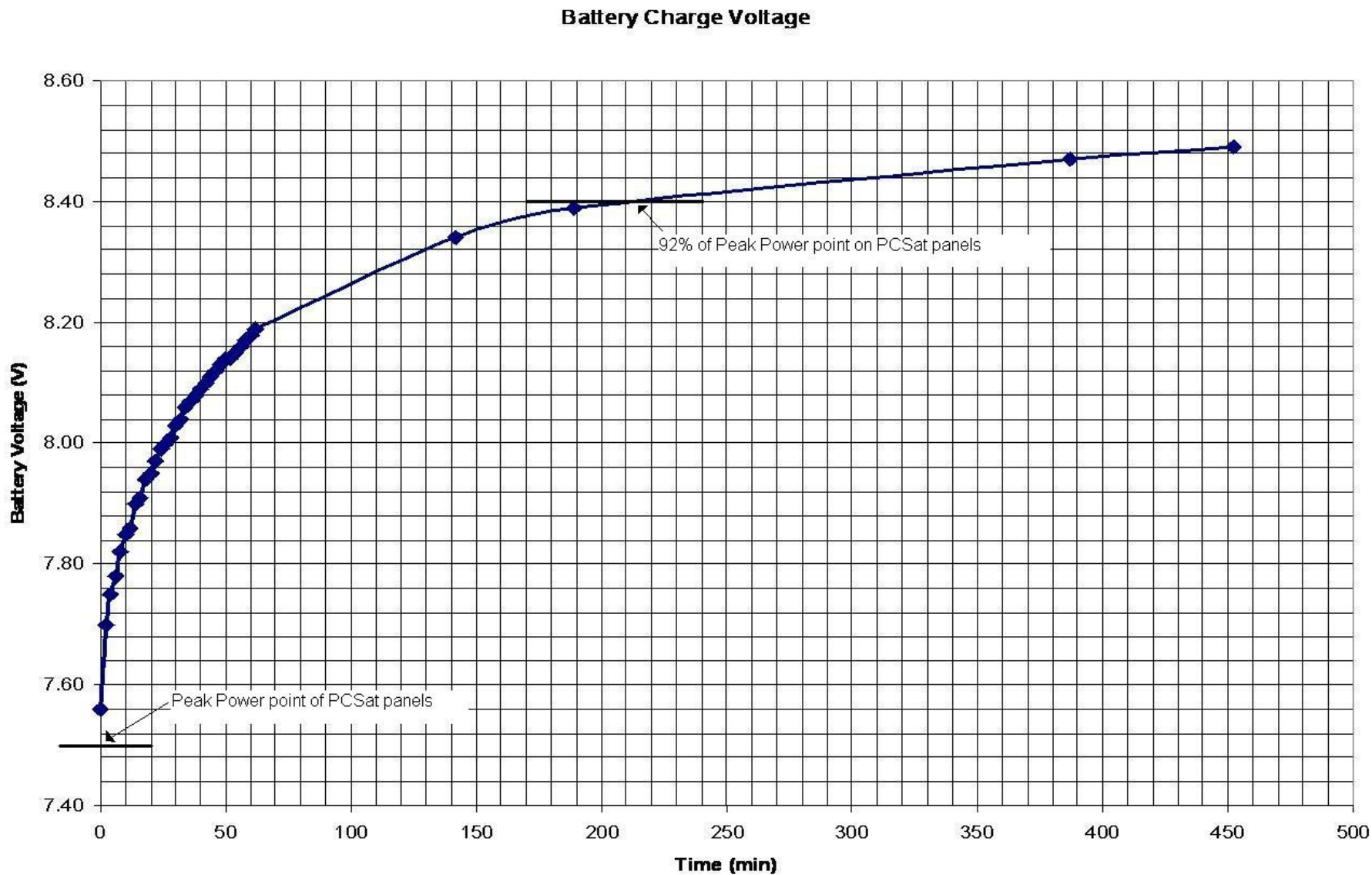
Dead Battery Recovery Test

Battery Charge Current

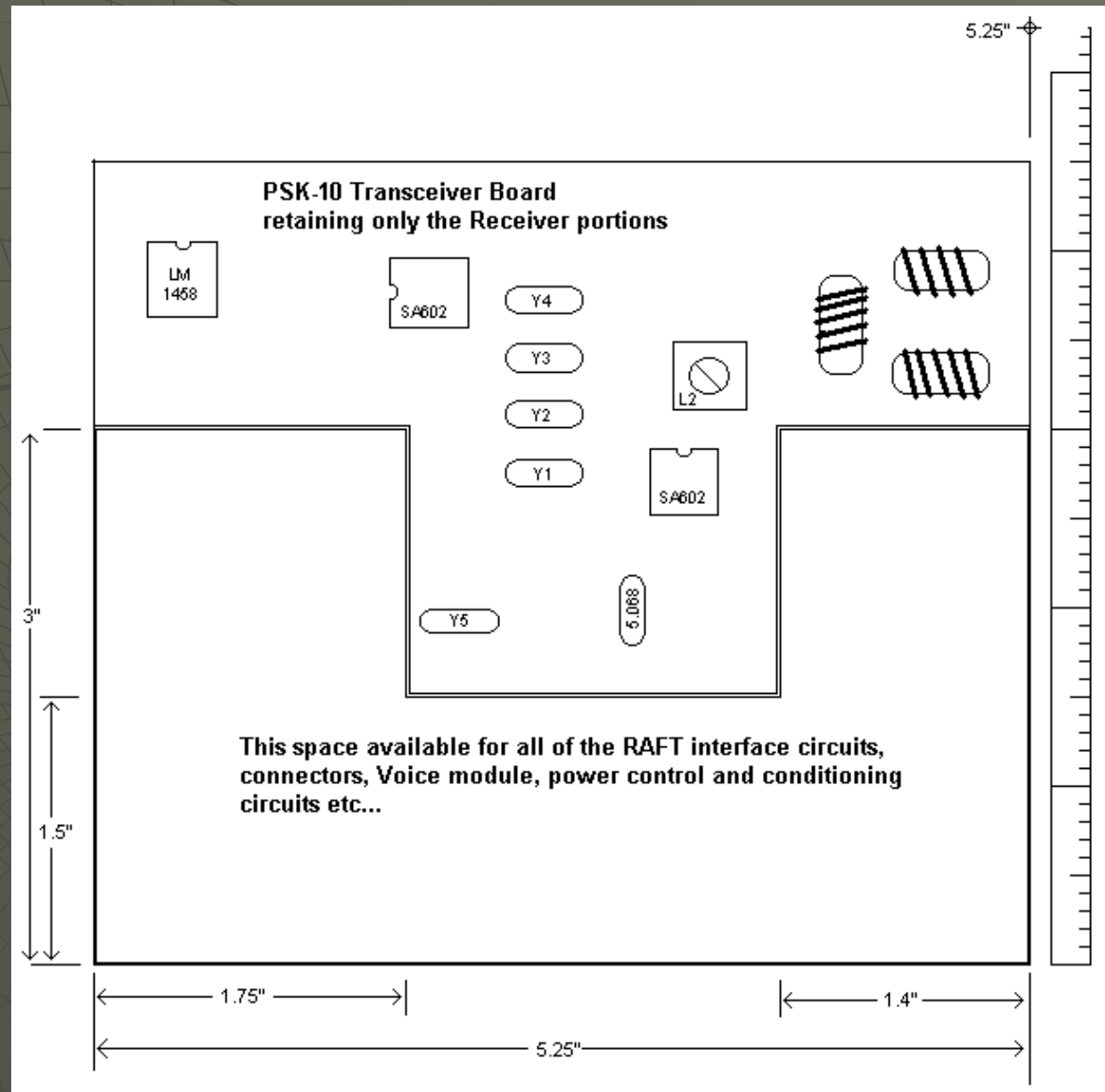
Driven by PCSat Cells I-V Curve



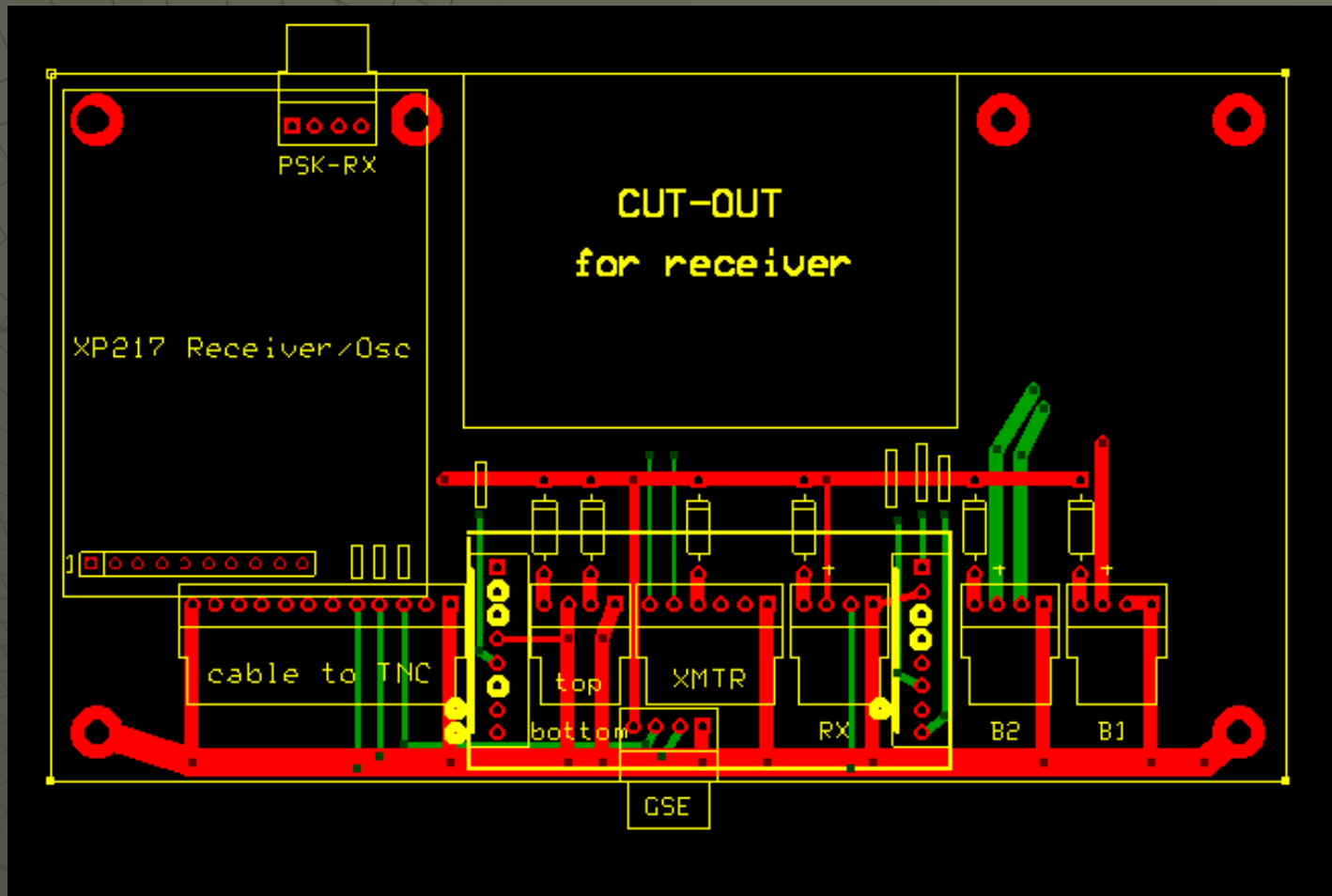
Dead Battery Charge Efficiency



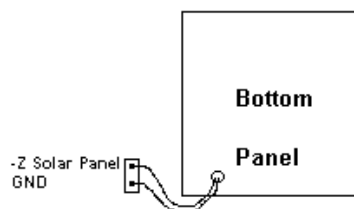
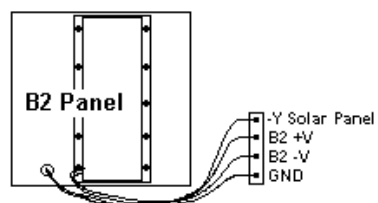
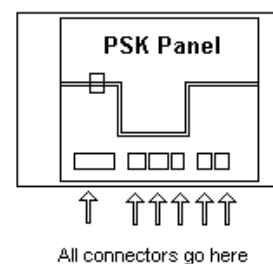
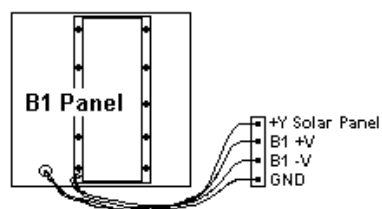
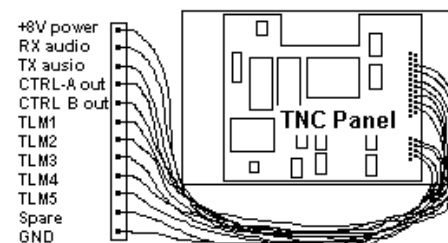
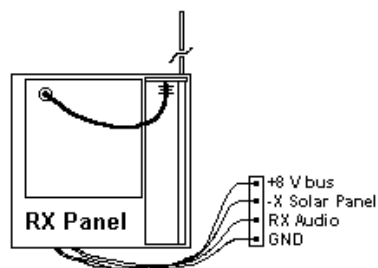
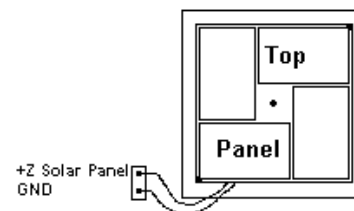
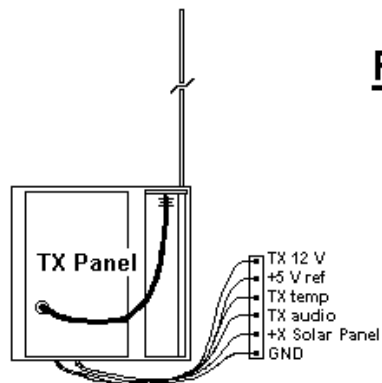
Interface Board



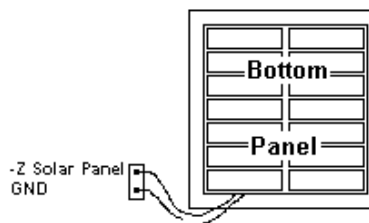
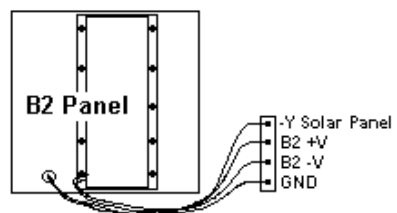
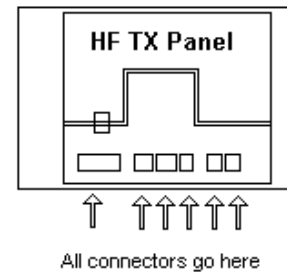
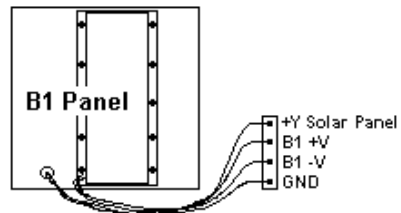
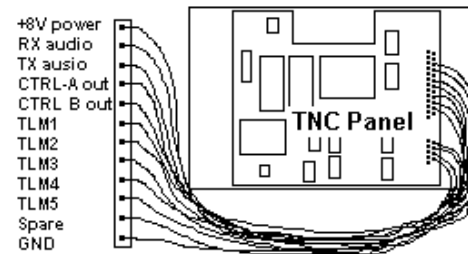
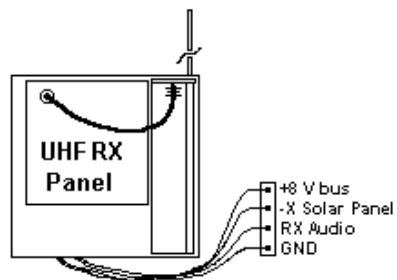
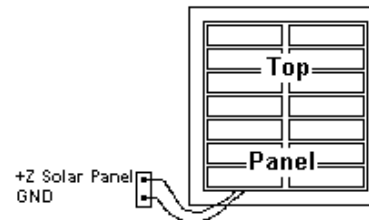
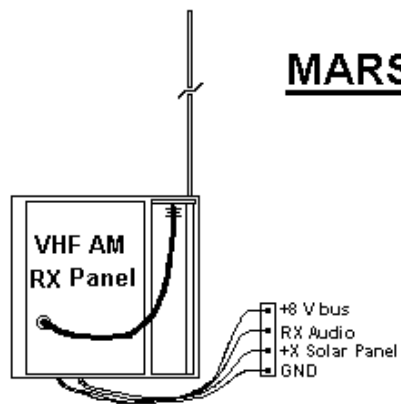
PCB Layout



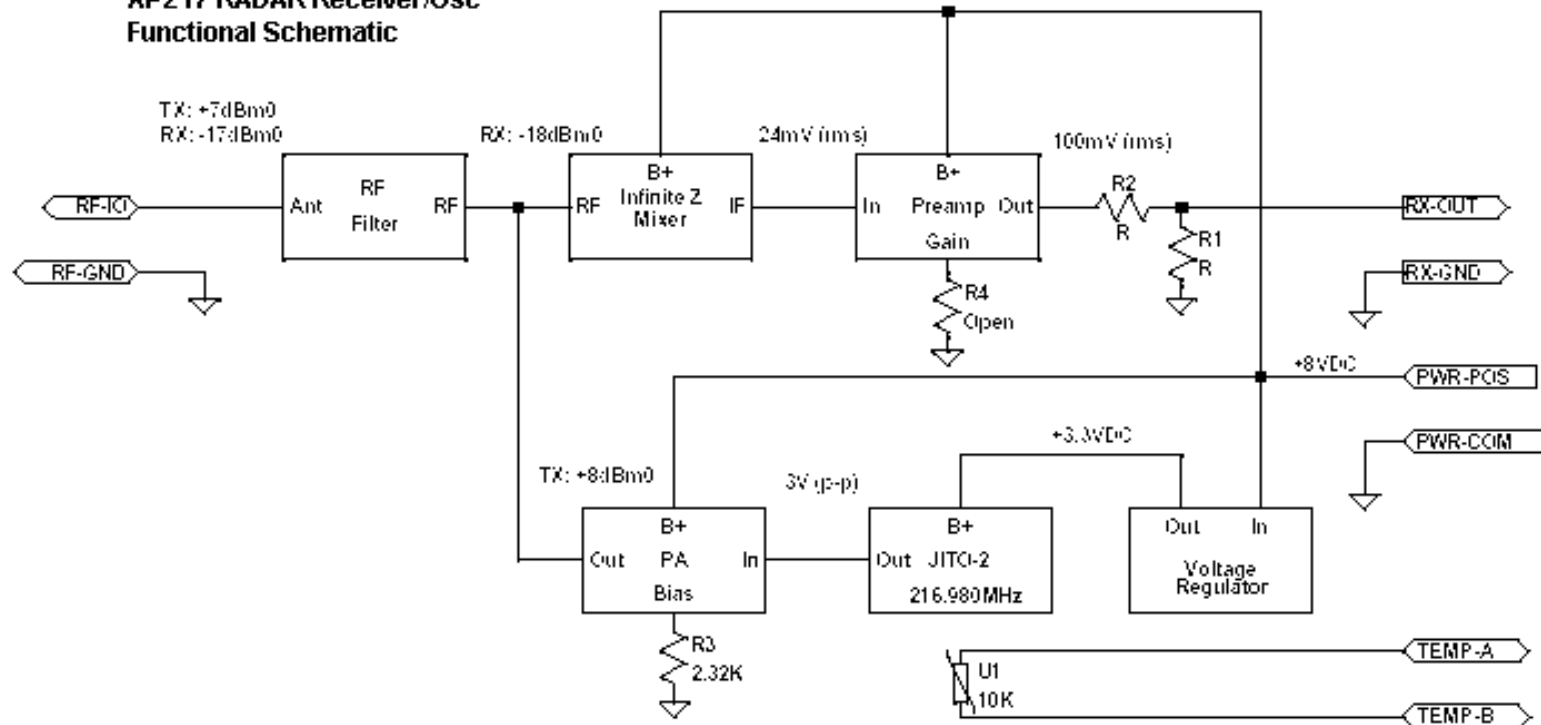
RAFT Panels and Connectors



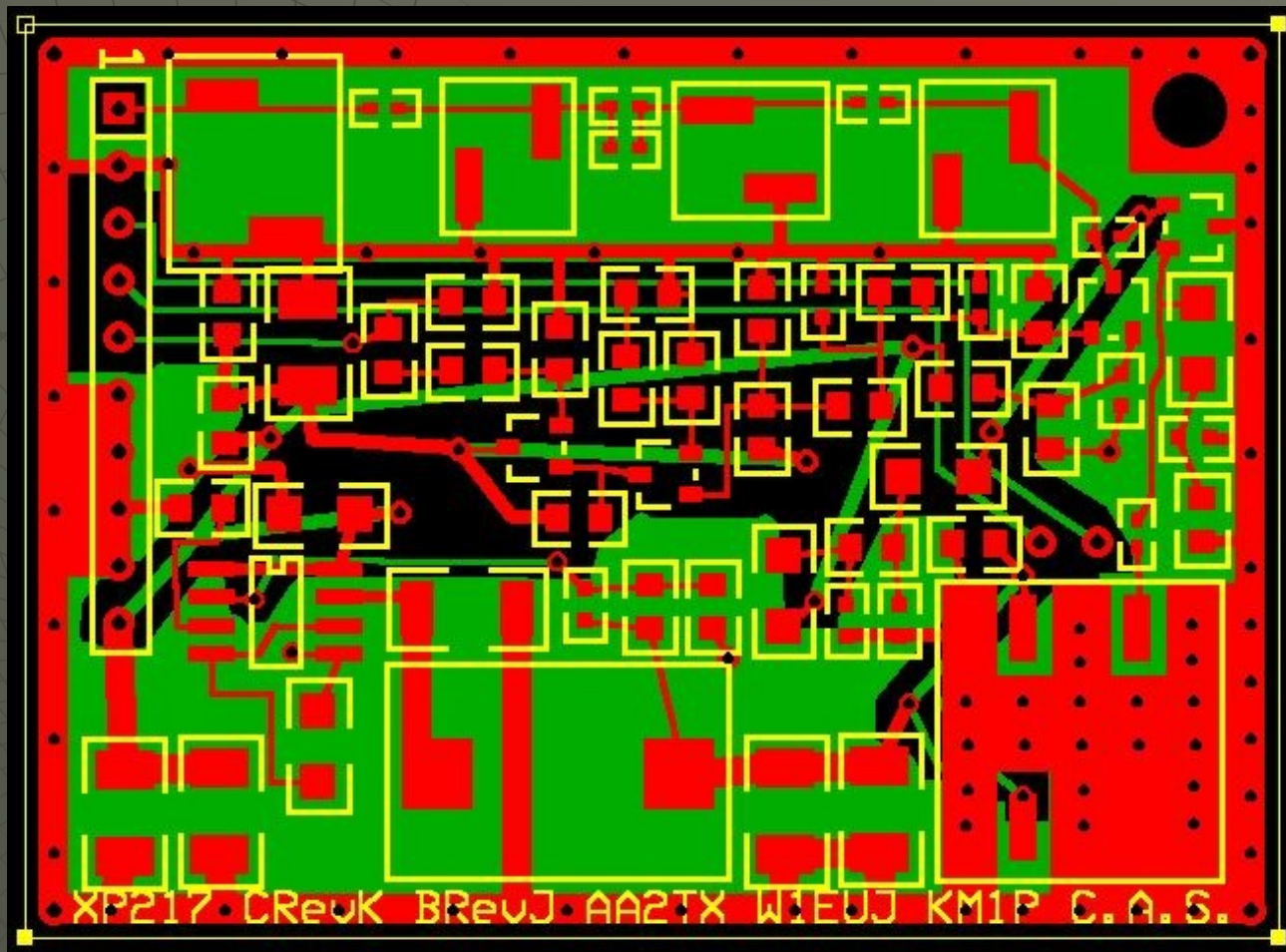
MARScom Panels and Connectors



XP217 RADAR Receiver/Osc Functional Schematic



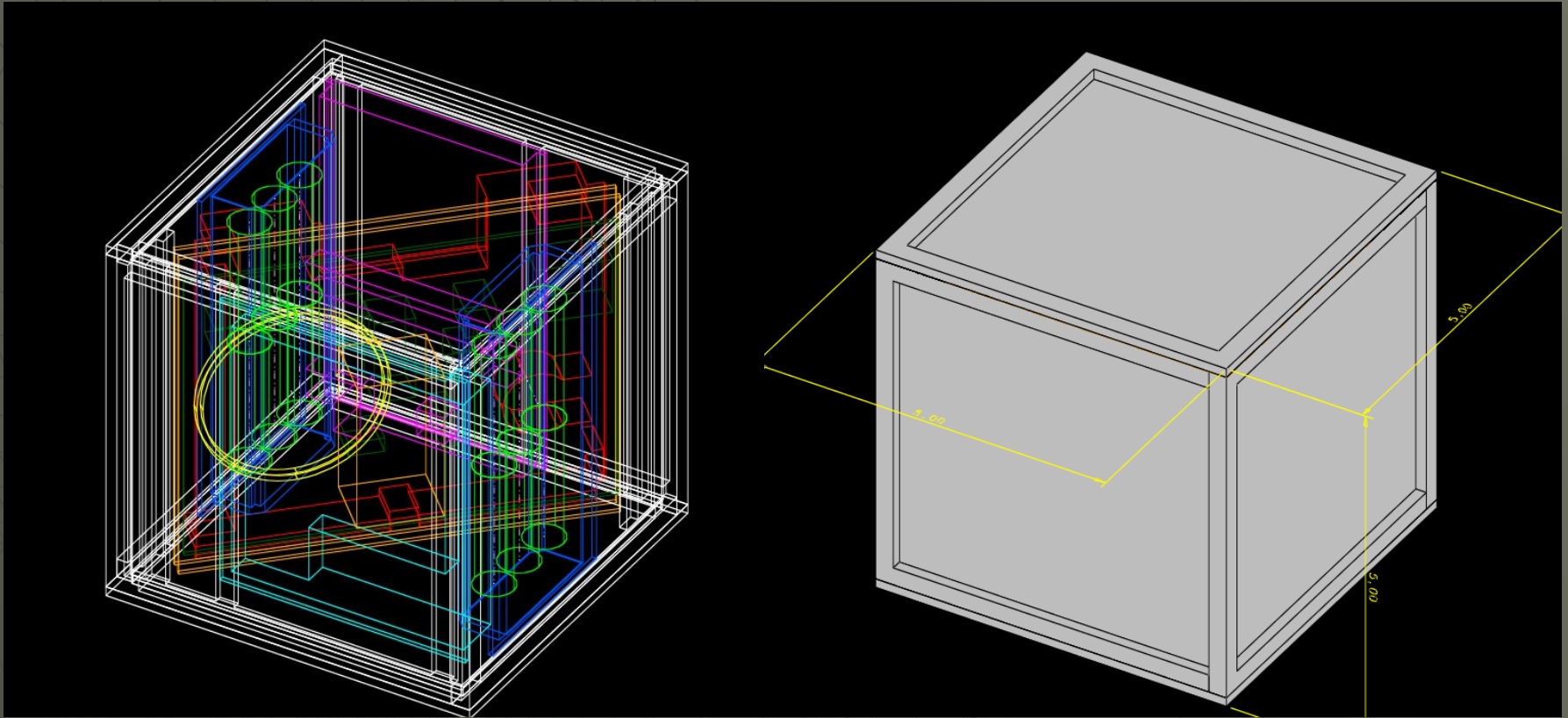
217Mhz Receiver PCB



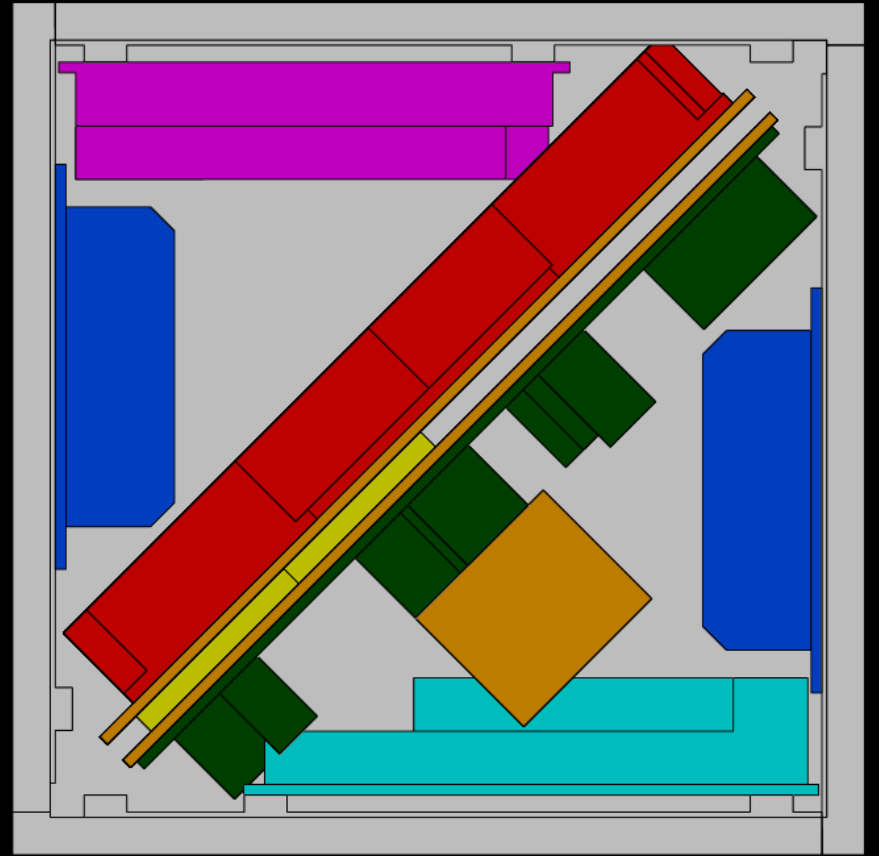
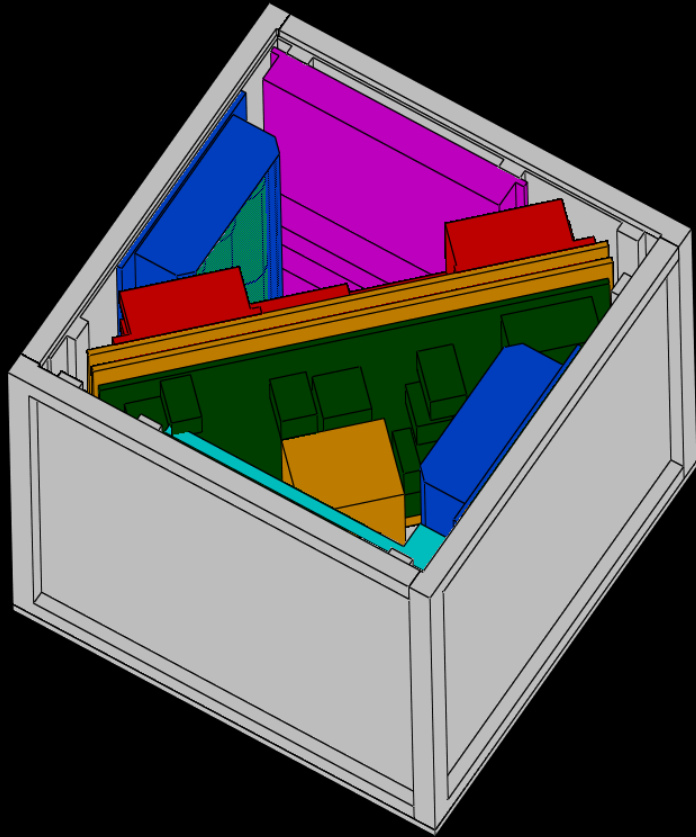
1.55in

2.175in

IDEAS Model



IDEAS Model



Communication

- ◆ RAFT1 requires an IARU Request Form
 - TX: 145.825 MHz, 2 Watt, 20 KHz B/W FM
 - RX: 29.400-29.403 MHz PSK-31 Receiver
 - RX: 145.825 MHz AX.25 FM
 - 216.98 MHz NSSS transponder
- ◆ MARScom requires a DD 1494
 - 148.375-148.975 MHz VHF cmd/user uplink
 - 24-29 MHz Downlink
 - 300 MHz UHF YP Craft Uplink Whip
 - ◆ Resonate at 216.98 MHz

VHF EZNEC Plot

W7EL EZNEC 2.0 RAFT1 VHF RX

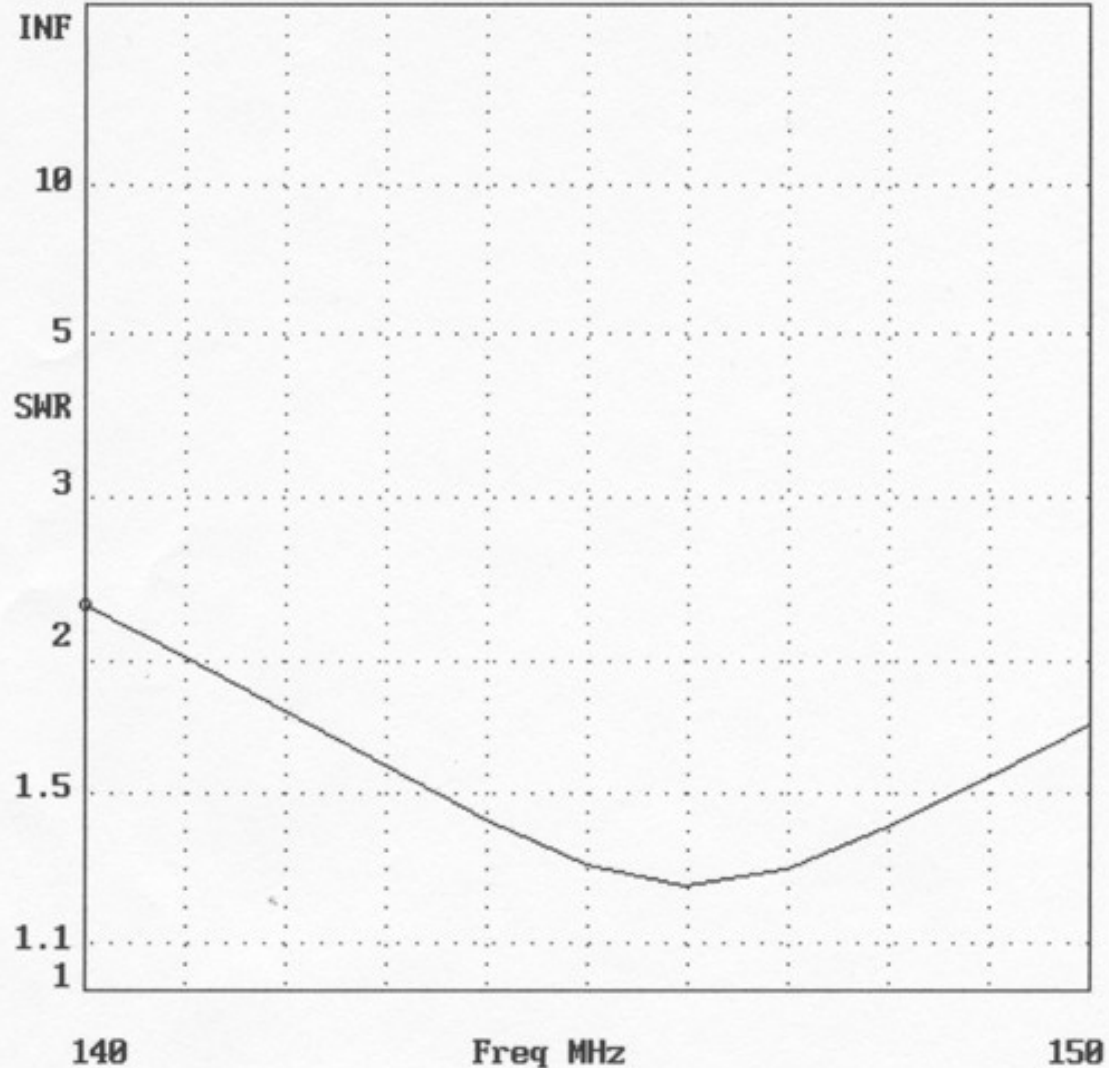
10-27-2004 11:47:26

← → Cursor pos INF
F Chg Freq range
M or F1 Menu on/off
P Print
U,<C>U Reverse colors
Z Chg SWR Z0
<ESC> Exit

Source # 1
Z0 = 50 ohms

Freq. = 140 MHz
SWR = 2.29

R = 44.03 ohms
X = -39.44 ohms

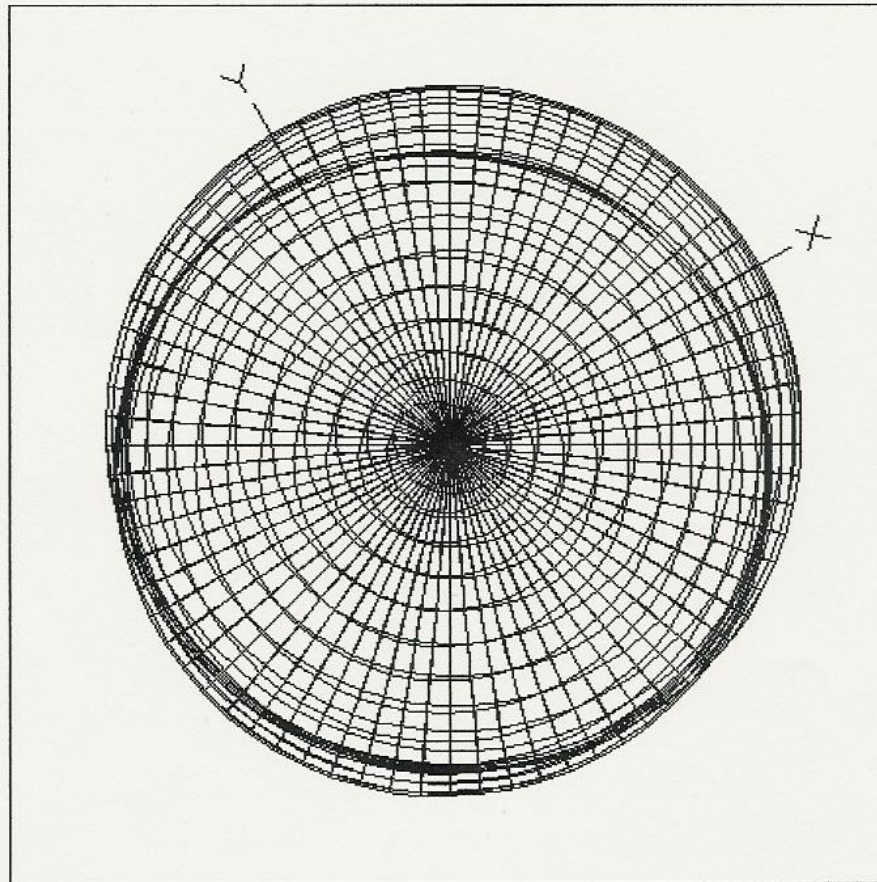


VHF EZNEC Plot

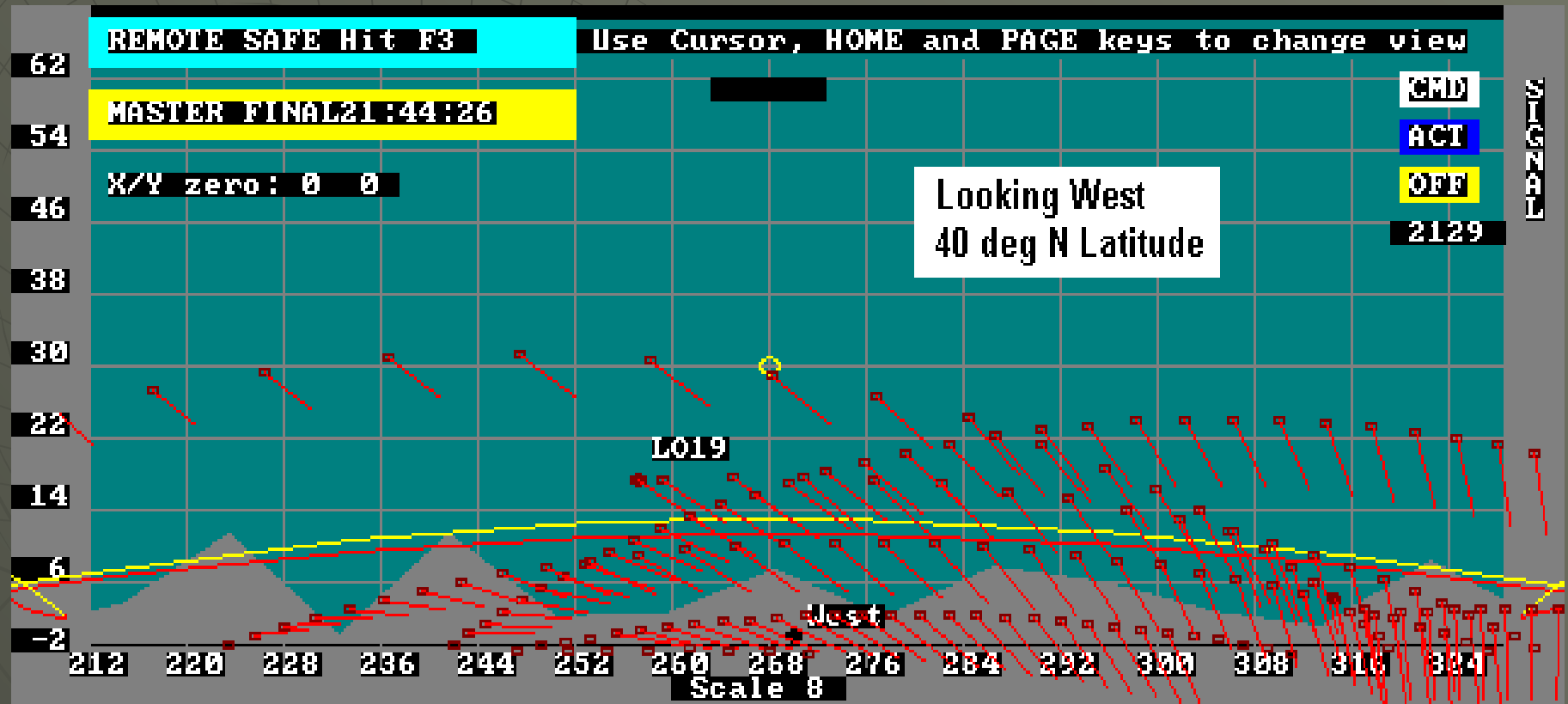
W7EL EZNEC 2.0 RAFT1 VHF RX

11-18-2004 20:59:20

↑→↓← Rotate
2 2D display
D Axes on/off
H Highlight slice
M or F1 Menu on/off
O Select colors
P Print
R, A Reset (All)
S Save 3D trace
V,<C>V Reverse colors
<A>XYZ View from axis
F2 NoFlash on/off
<ESC> Exit

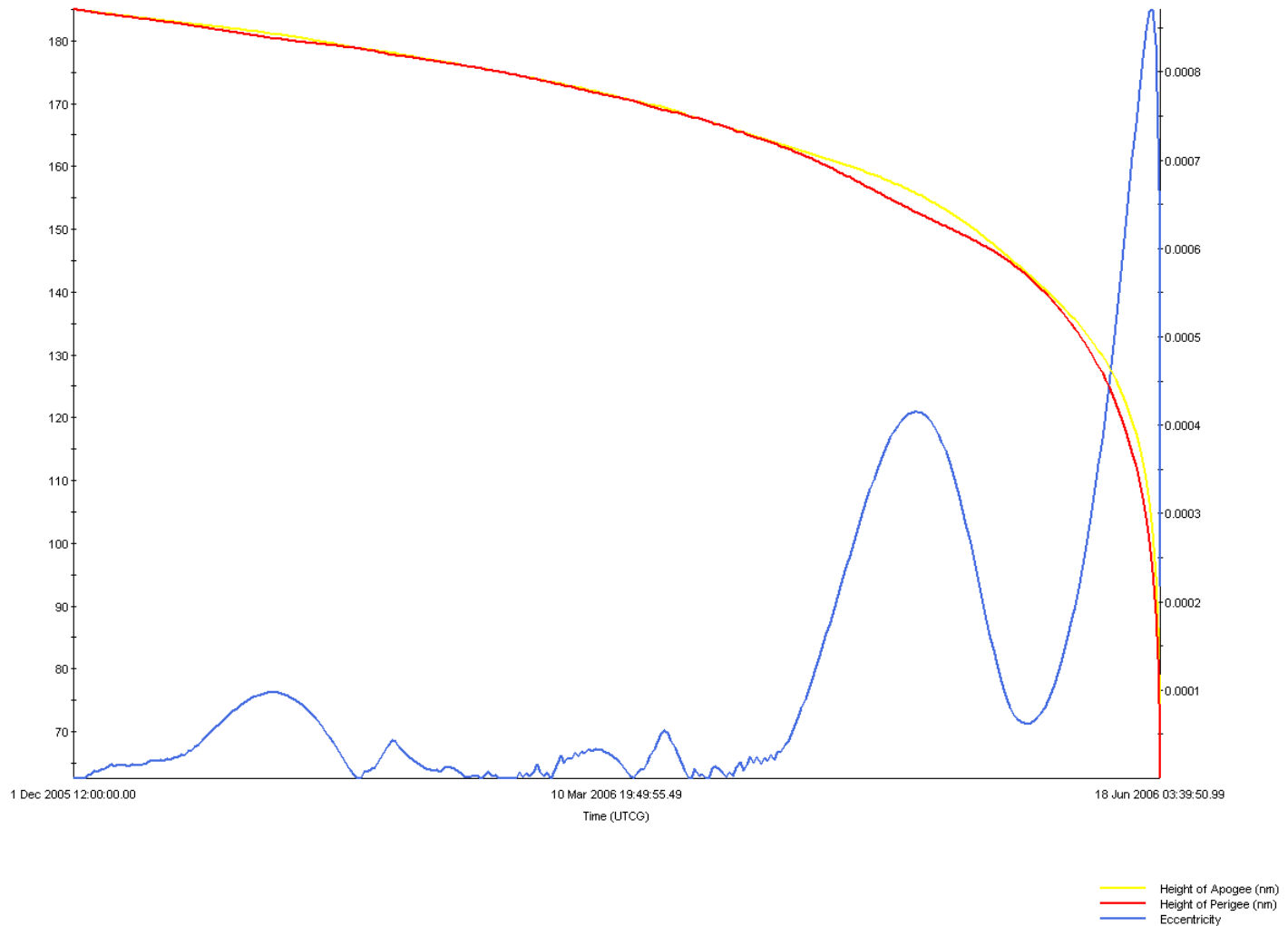


RAFT1 Magnetic Attitude Control

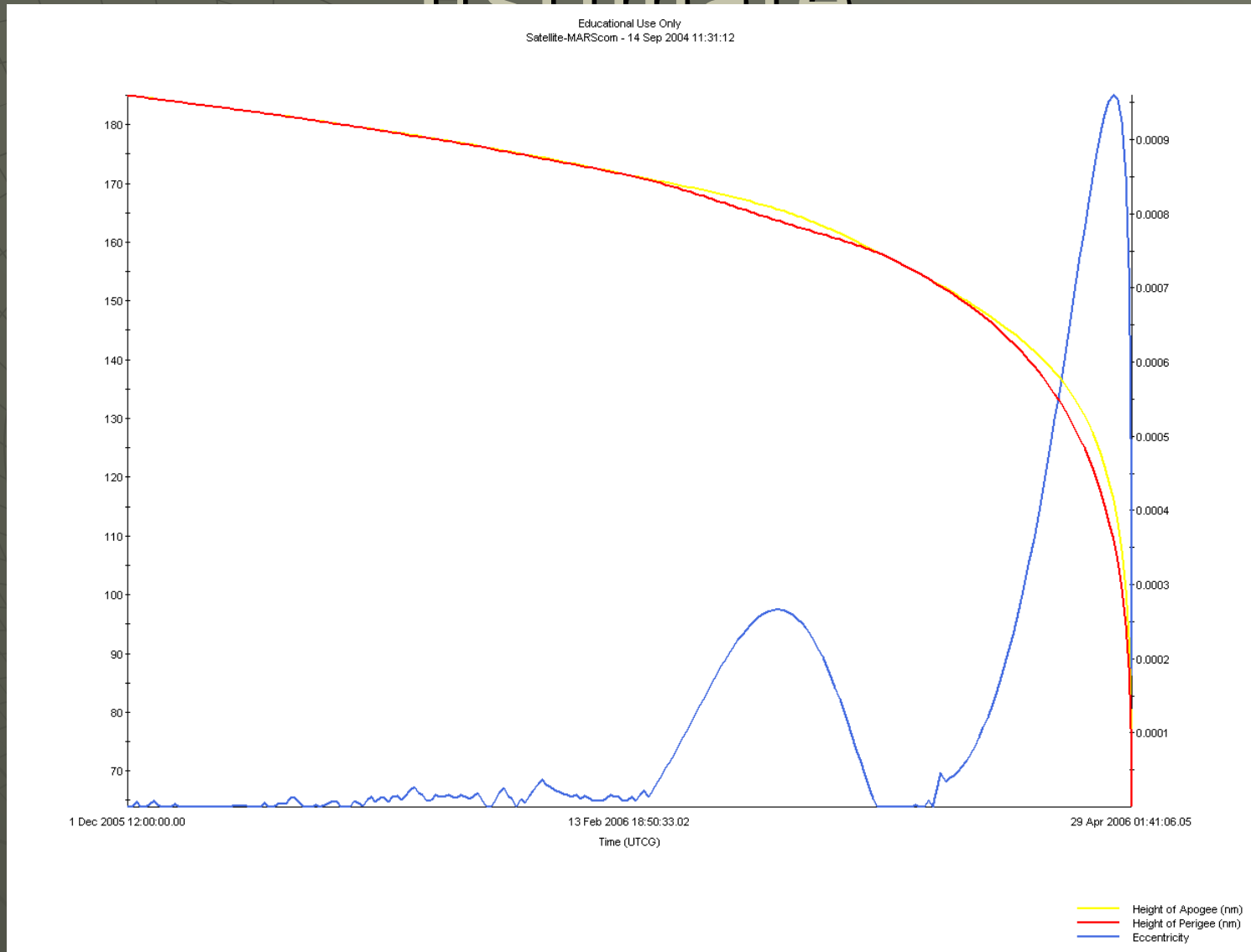


RAFT Lifetime Estimate

Educational Use Only
Satellite-RAFT - 14 Sep 2004 11:33:22



MARScOm Lifetime Estimate



Mass Budget (kg)

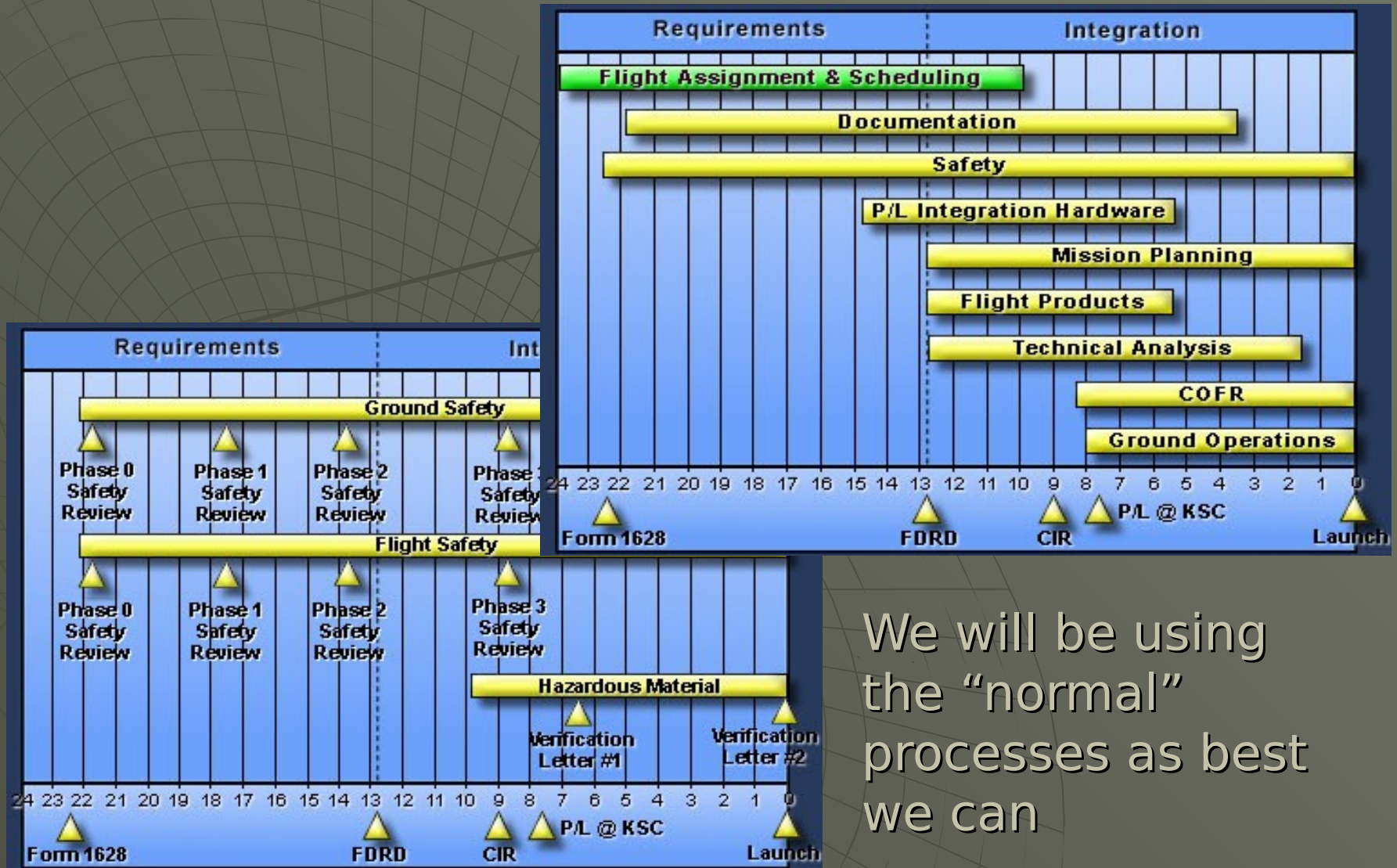
RAFT1

<u>Component</u>	<u>Mass (kg)</u>	<u>Comments</u>
Spool w/ HF Antenna	0.0536	Estimate
VHF Antenna	0.0046	Estimate
UHF Antenna	0.0046	Estimate
PSK-10 Board	0.1215	Includes Interface
TNC Board	0.1409	Actual
Interface Board	0	Estimated in PSK-10
Transmitter Board	0.0941	Actual
Receiver Board	0.083	Actual
Battery Boxes (2)	0.0406	Actual
AA Batteries (11)	0.2607	Actual
B1 Panel	0.138	Estimate
B2 Panel	0.138	Estimate
Transmitter Panel	0.138	Estimate
Receiver Panel	0.138	Estimate
Bottom Panel	0.138	Estimate
Top Panel	0.138	Estimate
PCSat Solar Panels (5)	0.3255	Actual
TOTAL	1.9571	
Max Allowed	4	

MARScom

<u>Component</u>	<u>Mass (kg)</u>	<u>Comments</u>
VHF FM RCVR	0.094	Estimate
VHF AM RCVR	0.094	Estimate
SSB Exciter	0.1	Estimate
1W Linear PA	0.04	Estimate
Splitter	0.04	Estimate
Decoder	0.04	Estimate
Batteries	0.168	Estimate
Ant/Spring combo	0.3	Estimate
20% Reserve	0.1752	Estimate
1/4" Aluminum	1.5	Estimate
Total	2.5512	
Max Allowed	3	

RAFT Integration & Safety



We will be using the “normal” processes as best we can

RAFT Schedule



Shuttle Safety Requirements

- ◆ Fracture Control Plan
- ◆ Fastener integrity
- ◆ A structural model of RAFT
- ◆ Venting analysis
- ◆ Simple mechanisms
- ◆ Materials compatibility / Outgassing
- ◆ Conformally coated PC boards
- ◆ Wire sizing and fusing
- ◆ Radiation hazard
- ◆ Battery safety requirements
- ◆ Shock and vibration

Battery Safety Requirements

- ◆ Must have circuit interrupters in ground leg
- ◆ Inner surface and terminals coated with insulating materials
- ◆ Physically constrained from movement and allowed to vent
- ◆ Absorbent materials used to fill void spaces
- ◆ Battery storage temperature limits are -30°C to $+50^{\circ}\text{C}$
- ◆ Prevent short circuits and operate below MFR's max
- ◆ Thermal analysis under load and no-load
- ◆ Battery must meet vibration and shock resistance stds
- ◆ Must survive single failure without inducing hazards
- ◆ Match cells for voltage, capacity, and charge retention

Key Requirement Documents

- ◆ Key Requirement Documents:
 - NSTS 1700.7B, Safety Policy and Requirements for Payloads Using the Space Transportation System
 - NSTS/ISS 18798, Interpretations of NSTS Payload Safety Requirements
 - NSTS/ISS 13830C, Payload Safety Review and Data Submittal Requirements
 - KHB 1700.7B, Space Shuttle Payload Ground Safety Handbook
 - NSTS 14046, Payload Verification Requirements
 - NASA-STD-5003, Fracture Control Requirements for Payloads using the Space Shuttle

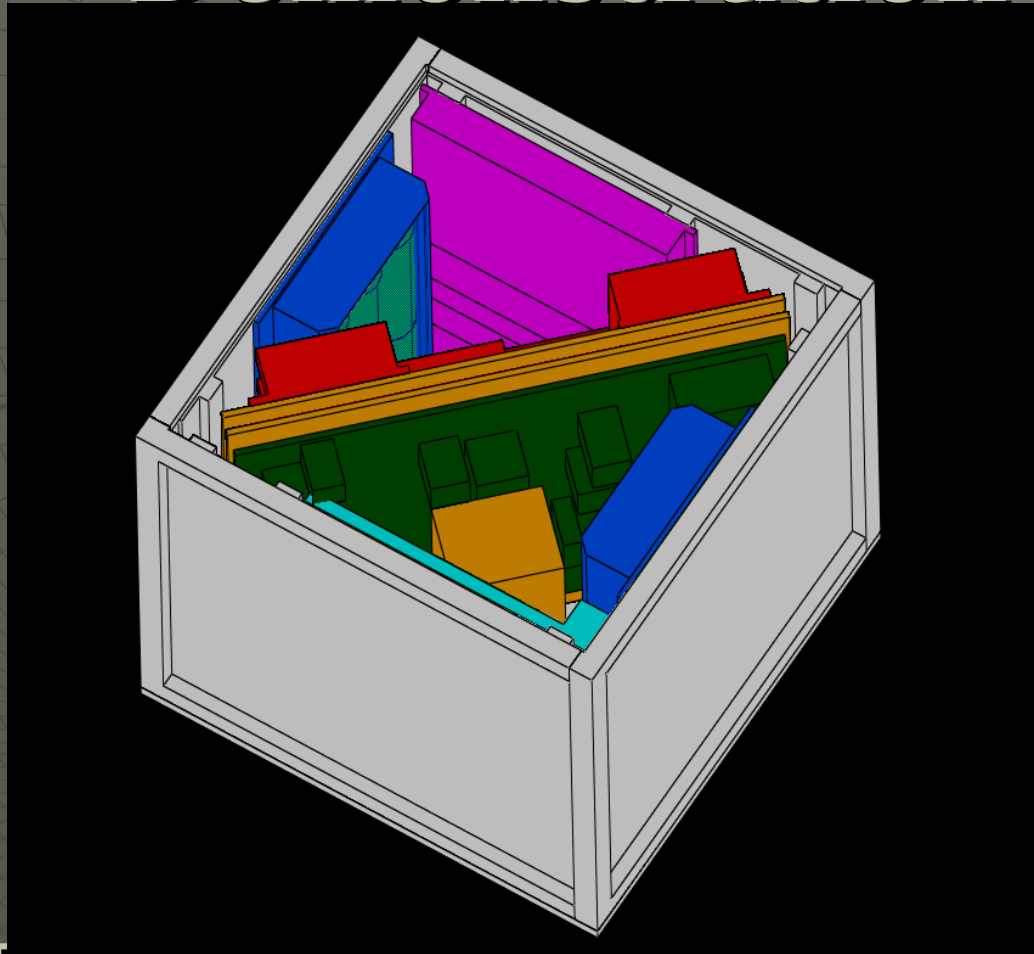
Key Reference Documents

- ◆ Reference/Requirements Documents (not all inclusive):
 - JSC 26943, Guidelines for the Preparation of Payload Flight Safety Data Packages and Hazard Reports
 - MSFC-STD-3029, Guidelines for the Selection of Metallic Materials for SCC Resistance
 - MSFC-HDBK-527/JSC 09604 (MAPTIS), Materials Selection List for Space Hardware Systems
 - JSC 20793, Manned Space Vehicle Battery Safety Handbook
 - TM 102179, Selection of Wires and Circuit Protective Devices for STS Orbiter Vehicle Payload Electrical Circuits

RAFT Schedule

- Systems Definition complete – 15 APR 2004
- Systems Requirement Baseline – 15 SEP 2004 (SRR)
- Prelim.Design Review– 19 NOV 2004
- Engineering Model Available– 15 JAN 2004
- System Design Complete – 15 FEB 2005 (CDR)
- Flight unit for Environmental testing – May 2005
- Flight Hardware for Integration/Flight – OCT 2005
- Launch – FEB 2005

IDEAS Model Demonstration



Located in Rickover
Computer Labs